

LRB

LIQUID ROCKET BOOSTER STUDY

ADDENDUM TO FINAL REPORT

AUGUST 31, 1990

CONTRACT NO. NAS8-37137
(MOD 10)

NATIONAL AERONAUTICS & SPACE ADMINISTRATION
MARSHALL SPACE FLIGHT CENTER
HUNTSVILLE, ALABAMA

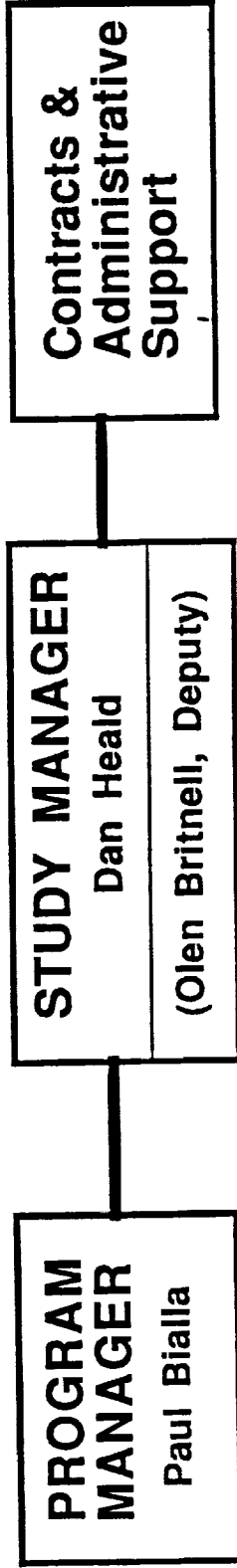
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LRB STUDY ORGANIZATION

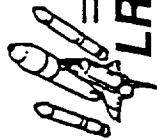


LRB



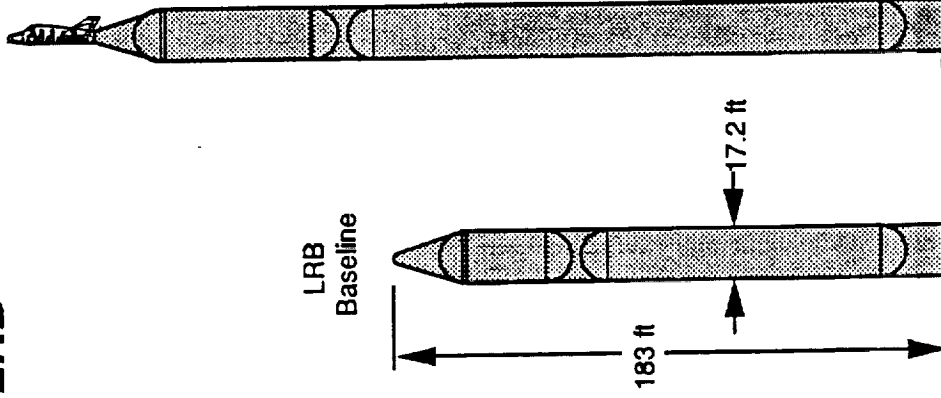
Terry Abel--Perf & Sizing	Vinod Shekher--Structures, Loads
John Beveridge--Propulsion	Jerry Shelby--Design, Launch Site Analysis
Hal Britton--Propulsion, Feedlines	Joe Szedula--Perf & Sizing, PLS Launcher Lead
Al Orillion--PLS Applications Lead	Richard Webb--Cost Analysis
John Burgeson--Design	Mike Vaccaro--Sys Eng, STS-C Lead
Gopal Mehta--Man-rating, Propulsion	

LRB LAUNCH VEHICLE CONCEPTS



LRB

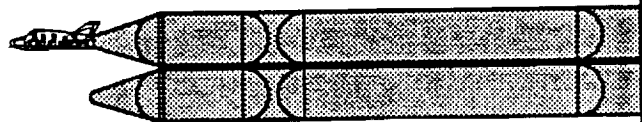
1 1/2 Stage



LRB
Baseline

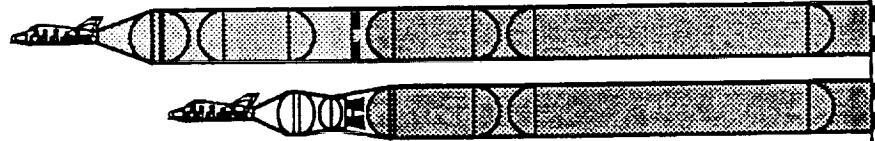
4 STE

Parallel
Stage



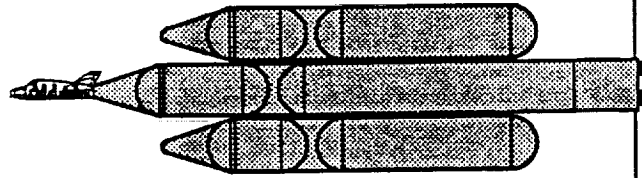
4 & 2 STE

Two Stage



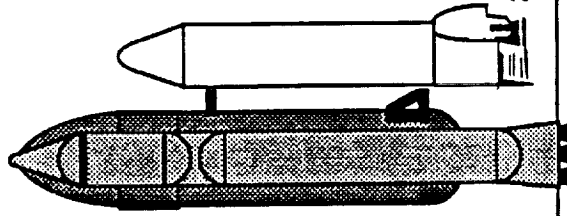
4 STE

Drop Tanks



4 STE

STS-C with
LRB booster & boattail



4 STE

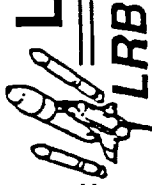
2 STE

Scale

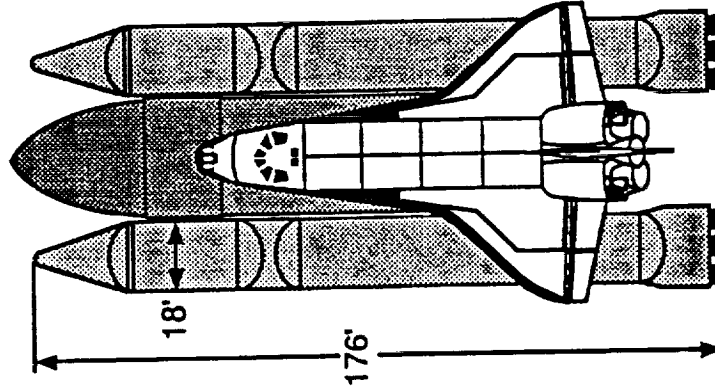
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CONCEPT SUMMARY

LO₂/LH₂ PUMP-FED WITH STE (JAN '90 DESIGN)



LRB



SELECTION RATIONALE

- CLEAN EXHAUST PRODUCTS; NON-TOXIC
- PROPELLANT COMMONALITY WITH STS LAUNCH
- SUBSTANTIAL EXPERIENCE BASE
- LIGHTEST GROSS WEIGHT IN CLASS
- NEW "LOW COST" ENGINE (STE)
- PREFERRED FOR ALTERNATE APPLICATIONS (ALS, STANDALONE)
- EXPENDABLE

PROGRAMMATIC DATA (1987 \$)*

- TOTAL NON-RECURRING COST: \$3,673 M
- AVERAGE UNIT COST, FOR 140 FLIGHTS: \$35.2M
- LIFE-CYCLE COST, FOR 10 YEARS: \$14,466M

ENGINE THRUST	LRB ASCENT PROPELLANT WEIGHT	SHUTTLE GLOW	THRUST/WEIGHT @L/O (NOMINAL)	ISP
510,475 (sl) 549,492 (v)	1,359,305	3,564,861	1.46	386 (sl) 415 (v)

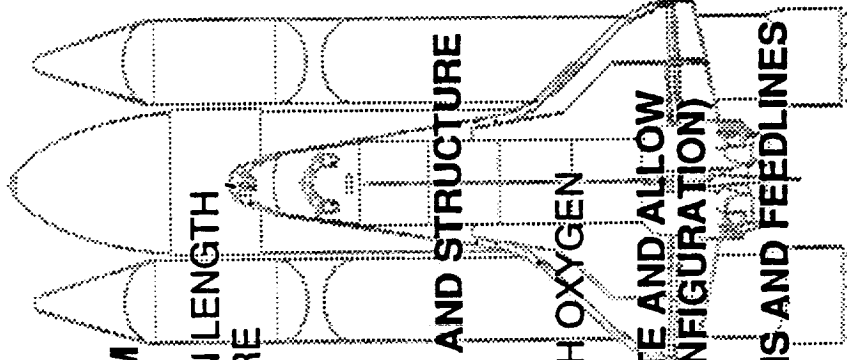
* EXCLUDES CONTRACTOR FEE, GOVERNMENT SUPPORT AND CONTINGENCY



LRB DESIGN IMPROVEMENTS

GENERAL DYNAMICS
Space Systems Division

- RESOLVED FORWARD ATTACH POINT PROBLEM
 - SIZE WAS 17.2 FT IN DIAMETER BY 183 FT IN LENGTH
 - ATTACH POINT IS IN INTERTANK STRUCTURE
- ADOPTED STE AS BASELINE ENGINE
 - 20:1 EXPANSION RATIO
- ADOPTED 2090 AL-LI AS MATERIAL FOR TANKS AND STRUCTURE
 - 7% WEIGHT SAVINGS
 - RECENT NASA ACCEPTANCE FOR USE WITH OXYGEN
- REDESIGNED AFT SKIRT TO ACCOMMODATE STE AND ALLOW FOR CLOSE MOUNTING OF LRB (PARALLEL CONFIGURATION)
- REFINED WEIGHT ESTIMATES FOR SUBSYSTEMS AND FEEDLINES



BASELINE LRB (APRIL '90 DESIGN)



LRB

Design Goals:

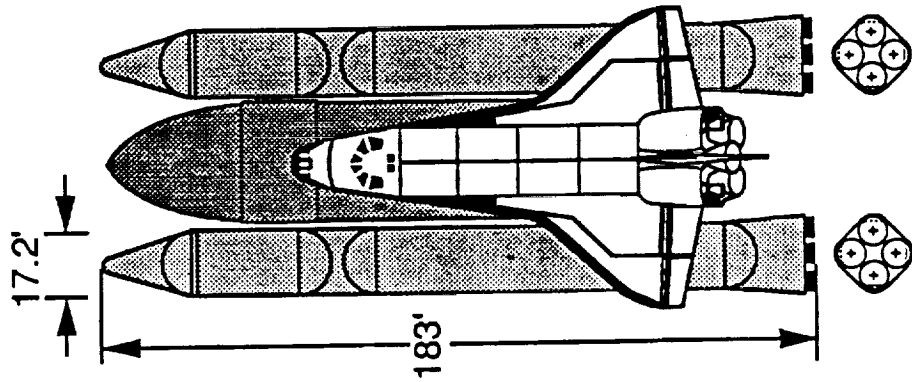
Safe abort at any point in trajectory
ATO Capability with single LRB engine out at lift off
Minimum impacts to current STS

Weights (lbs):

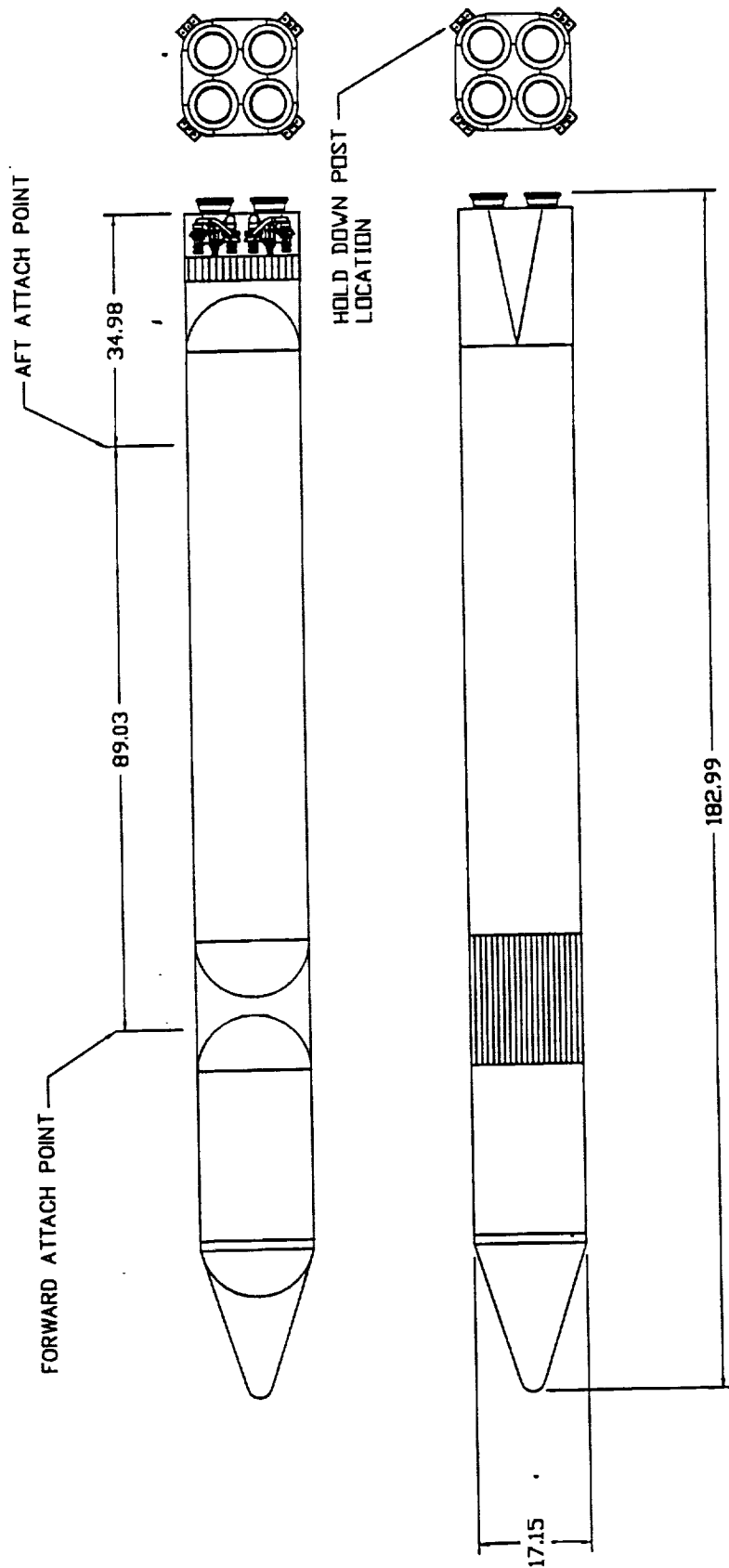
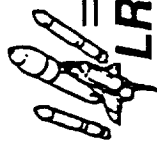
Payload 70,500
LRB Dry Weight 113,039
LRB Inert Weight 123,141
LRB Ascent Propellant 655,640
LRB GLOW 788,781
STS/LRB GLOW 3,521,797

LRB Propulsion:

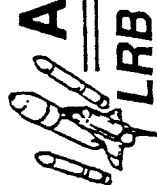
Number of engines per LRB 4
Engine type STE
Area Ratio 20:1
Vacuum Thrust (lbs) 558,542
Sea Level Thrust (lbs) 514,232
Vacuum Isp (sec) 413
Sea Level Isp (sec) 380



LIQUID ROCKET BOOSTER BASELINE WITH STE ENGINES

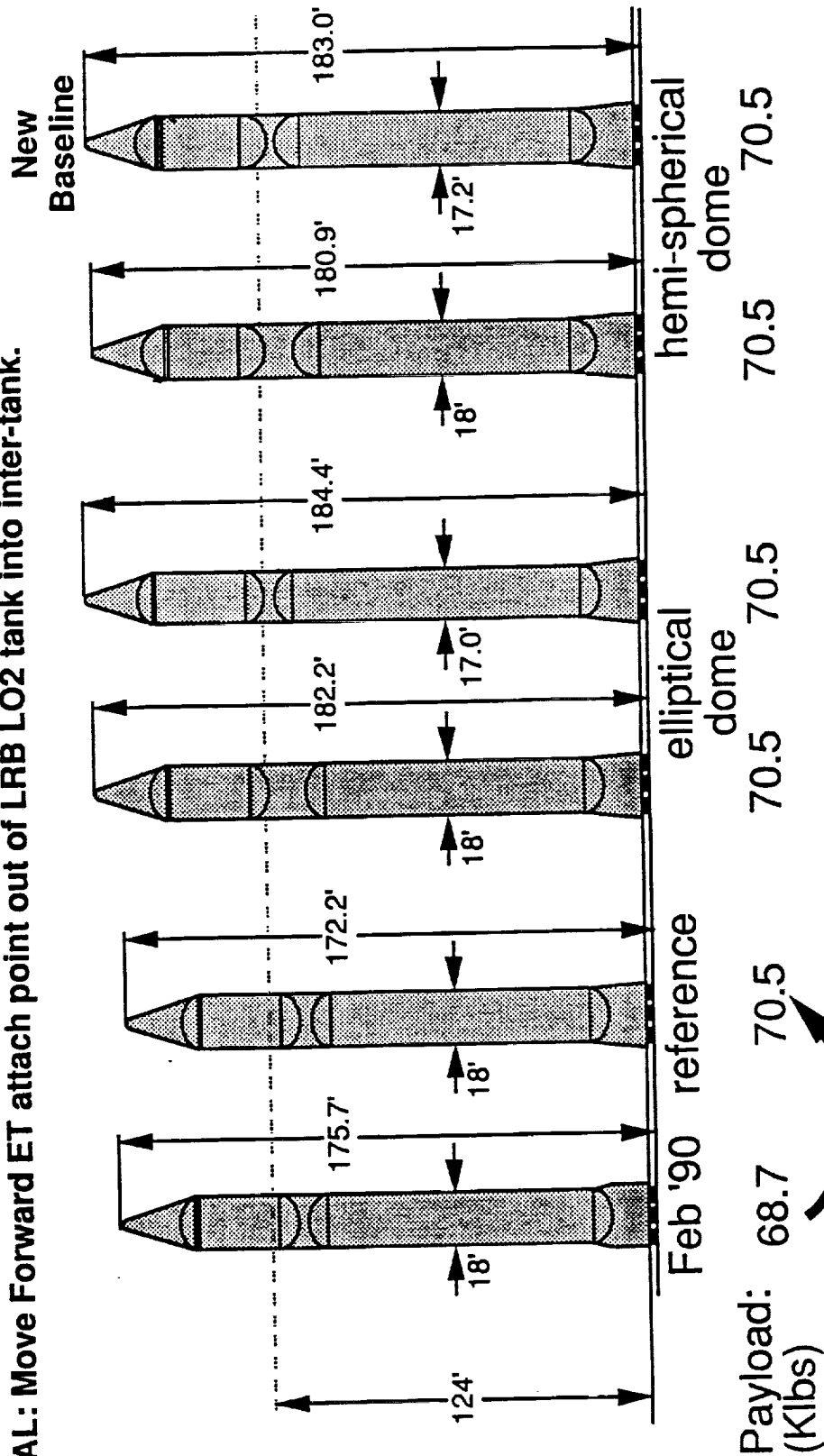


ATTACH POINT SOLUTIONS



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GOAL: Move Forward ET attach point out of LRB LO2 tank into inter-tank.



materials,
updated systems,
additional systems

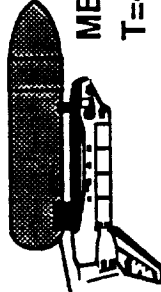
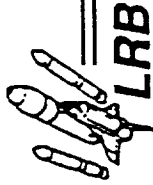
LRB USING STE20 vs. STE40



Question: What are the advantages/disadvantages of modifying STEs for a STS LRB?

	STE20	STE40
Nozzle Area Ratio	20:1	40:1
Payload (lbs)	70,500	62,690
LRB Length (ft)	183.0	182.6
LRB Diameter (ft)	17.2	16.8
Aft Skirt:	Square with rounded corners, permits side-by-side LRB placement	Flared, requires large attach beam for side-by-side LRB placement
Engine:	Requires STE to have two nozzle designs but can use common combustion chamber and turbo pumps	Single STE design

ABORT CAPABILITY



MECO
T=495.8: Nominal
T=497.4: Earliest STE shutdown
T=476.8: ATO
T=544.2: Make mission with SSME out
T=572.0: ATO with SSME out

Make Mission with single SSME out
T=366.7: Make mission with SSME out

ATO with single SSME out
T=301.8: ATO with SSME out

LRB Separation

T=151.4: Nominal
T=154.8: Earliest STE shutdown
T=163.8: ATO

Make Mission with single LRB engine out

T=37.1: Nominal
T=27.1: Earliest STE shutdown

T=3.9: SSMEs to 104% @ 60 ft/sec (not performed if engine out at T=0)

T=0: ATO capability with single LRB engine out & 70,500 lbs payload

Lift-off: SSMEs at 100%, LRB STEs at 100%

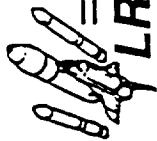
LRB DERIVED PLS LAUNCH VEHICLE STUDY ACTIVITIES



OBJECTIVE

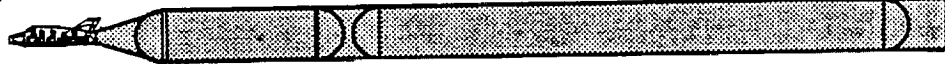
- Evaluate Options of Developing a PLS Launch Vehicle (LV)
 - Utilize LRB
 - Optimize from LRB
- Determine the Best Commonality and Cost Effective Concept

LRB LAUNCH VEHICLE CONCEPTS



LRB

1 1/2 Stage



2 x 2 STE

LRB
Baseline

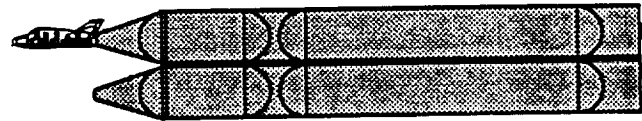


4 STE

183 ft

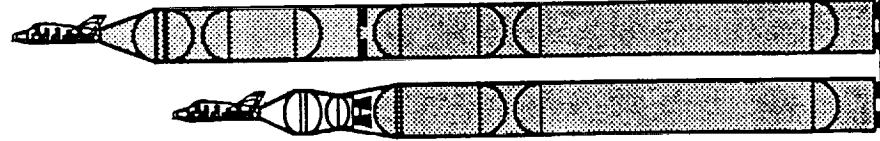
17.2 ft

Parallel
Stage



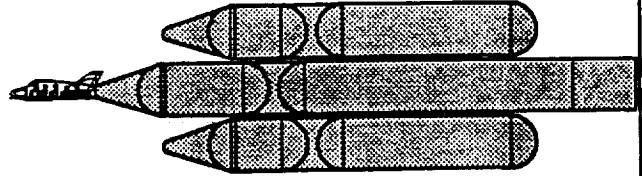
4 & 2 STE

Two Stage



4 STE

Drop Tanks



4 STE



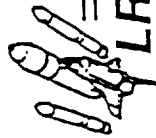
LV FOR PLS STUDY PLAN



APPROACH

- Utilize the LaRc 10 Man PLS as Basic Concept
- Conduct Trade Analyses on four LV from LRB concepts:
 - 1) 1 1/2 Stages
 - 2) Parallel
 - 3) 2 Stages (2nd Stg = Centaur & LRB)
 - 4) Drop Tanks
- Evaluate for PLS Insertion Orbits, nmi, of:
 - A) 50 X 100
 - B) 39 X 217 (SSF Transfer Orbit)
 - C) 220 X 220 (2 Stage only)

PLS LV OPTIONS & COMMONALITIES CONSIDERATIONS



LRB

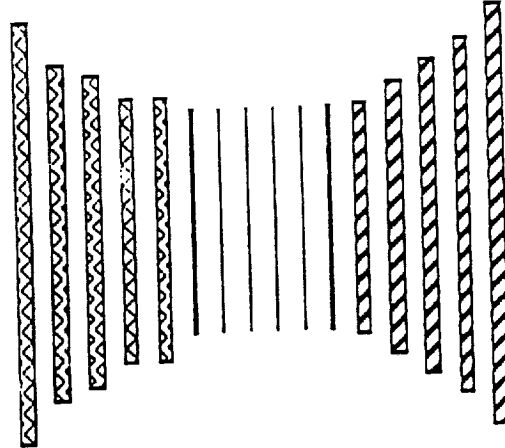
LV OPTIONS: • 1/2 Stages • Parallel Stages • 2 Stages • Drop Tanks

LEVEL OF COMMONALITY - LRB TO LV IMPACTS

Increases Changes In

- Tank Wall Thk
- Wp/Tank Sizes
- Structures
- STE Requirements
- KSC Impacts

Commonality - LRB to LV

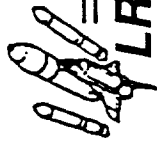


Range of Best
Compromise
Concept

Optimized - LV from LRB

PLS LV

GROUND RULES AND CONSTRAINTS



LRB

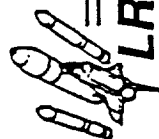
PLS

- | | |
|---|-------------|
| • LaRc 10 Man Orbiter, Wt | = 22,744 lb |
| • Adapter (initial) W/Escape System, Wt | = 10,543 |
| | ----- |
| Lift Off, payload Wt | = 33,287 lb |

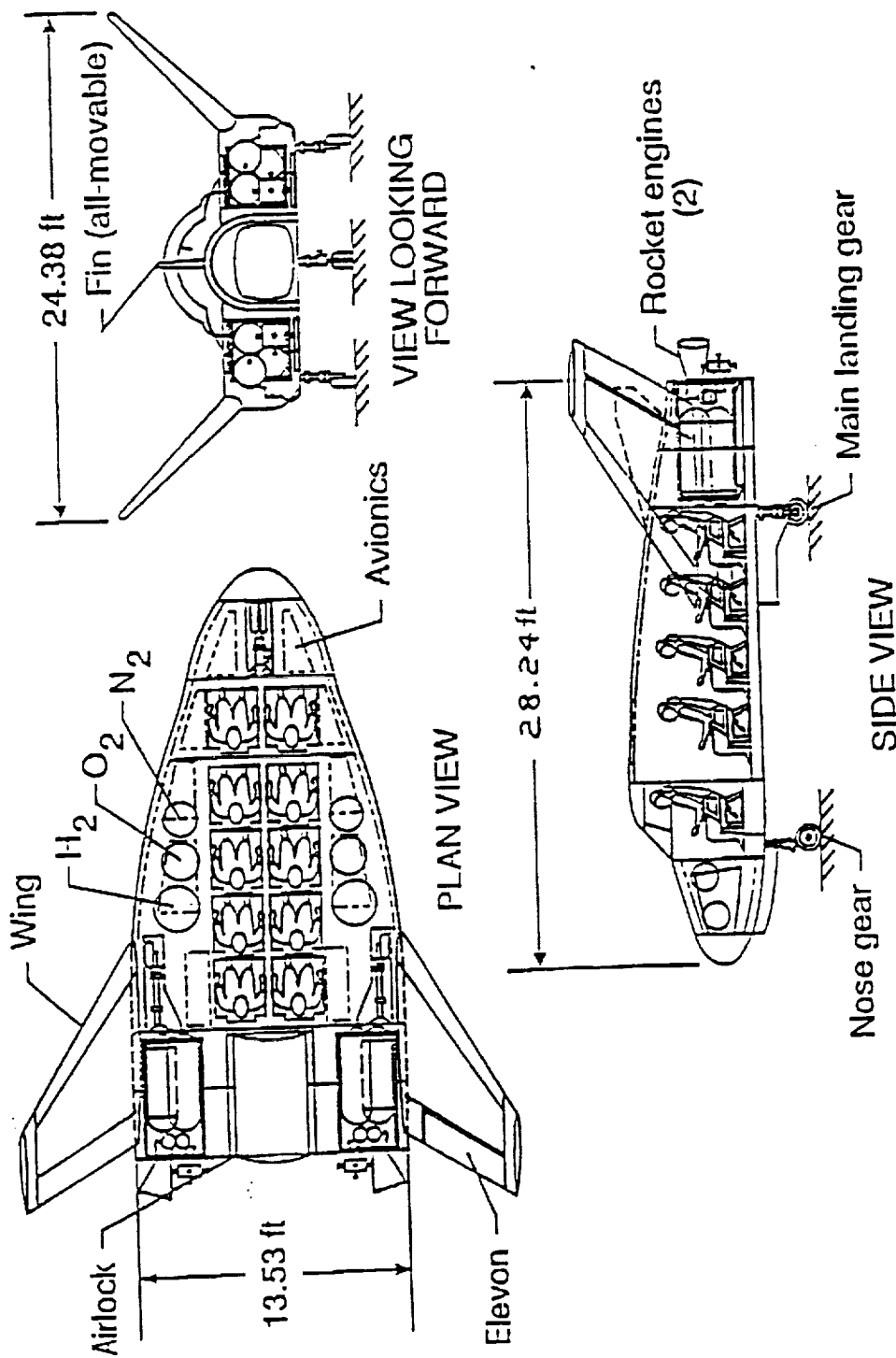
LRB LAUNCH VEHICLES FOR PLS

- Boosters = LRB materials and STEs
- 2nd Stage Engines = RL-10 for Centaur and STE for LRB Derivative
- 2nd Stage to have Controlled Reentry from 220 X 220 Nmi Orbit
- Avionics for G&N = GD Adaptive G & N Type
- Trajectory Constraints: Max q = 850 psf; Max g = 3

LaRc 10 MAN PLS

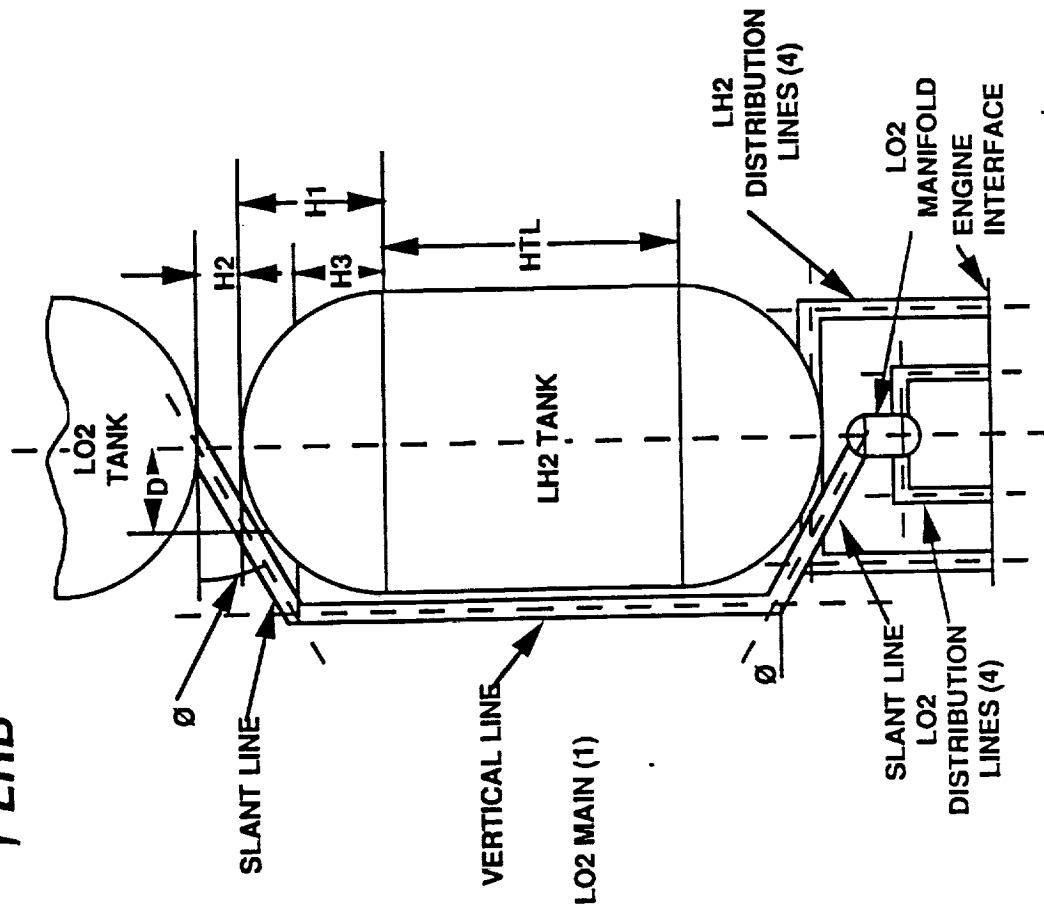
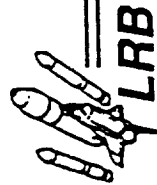


LRB



BASELINE PROPELLANT FEED SYSTEM

GENERAL DYNAMICS
Space Systems Division



FEEDLINES		
	LENGTH inches	I.D. WEIGHT inches pounds
L02		
MAIN FEED		22
SLANT LINES		
INTERTANK	103.8	
AFT SKIRT	88.8	
VERTICAL RUN	1236.9	
MANIFOLD		123
DISTRIBUTION LINES - 4 REQD.		
HORIZONTAL RUN	26.4	12
VERTICAL RUN	29.3	
LINE WEIGHT		1393
COMPONENTS WEIGHT		1504
FLEX JOINTS - 3		22
FLEX JOINTS - 1		12
GIMBAL JOINT - 1		12
PREVALVE		12
L02 TOTAL WEIGHT		3020
LH2		
DISTRIBUTION LINES - 4 REQD.		12
HORIZONTAL RUN	86.4	
VERTICAL RUN	81	
LINE WEIGHT		82
COMPONENTS WEIGHT		1000
FLEX JOINTS - 1		12
GIMBAL JOINTS - 1		12
LH2 TOTAL WEIGHT		1328
SYSTEM TOTAL WEIGHT		4348

BASELINE PROPULSION SUPPORT SYSTEMS



LRB

VENT SYSTEM - DUCTED TO MLP QD

LINE LENGTHS
LO2 2114 inches
LH2 1561 inches

LINE WEIGHTS
LO2 524 lbs
LH2 387 lbs

COMPONENT WEIGHT PER LINE 209 lbs

TOTAL WEIGHTS
LO2 733 lbs
LH2 596 lbs

SYSTEM TOTAL 1329 lbs

PRESSURIZATION SYSTEM

LINE LENGTHS
INTERNAL 73 inches
EXTERNAL
LO2 2062 inches
LH2 1509 inches

LINE WEIGHTS
INTERNAL 27 lbs
EXTERNAL
LO2 143 lbs
LH2 127 lbs

TOTALS
LO2 266 lbs
LH2 250 lbs

SYSTEM TOTAL 515 lbs

PNEUMATIC SYSTEM

ESTIMATED FROM ORBITER

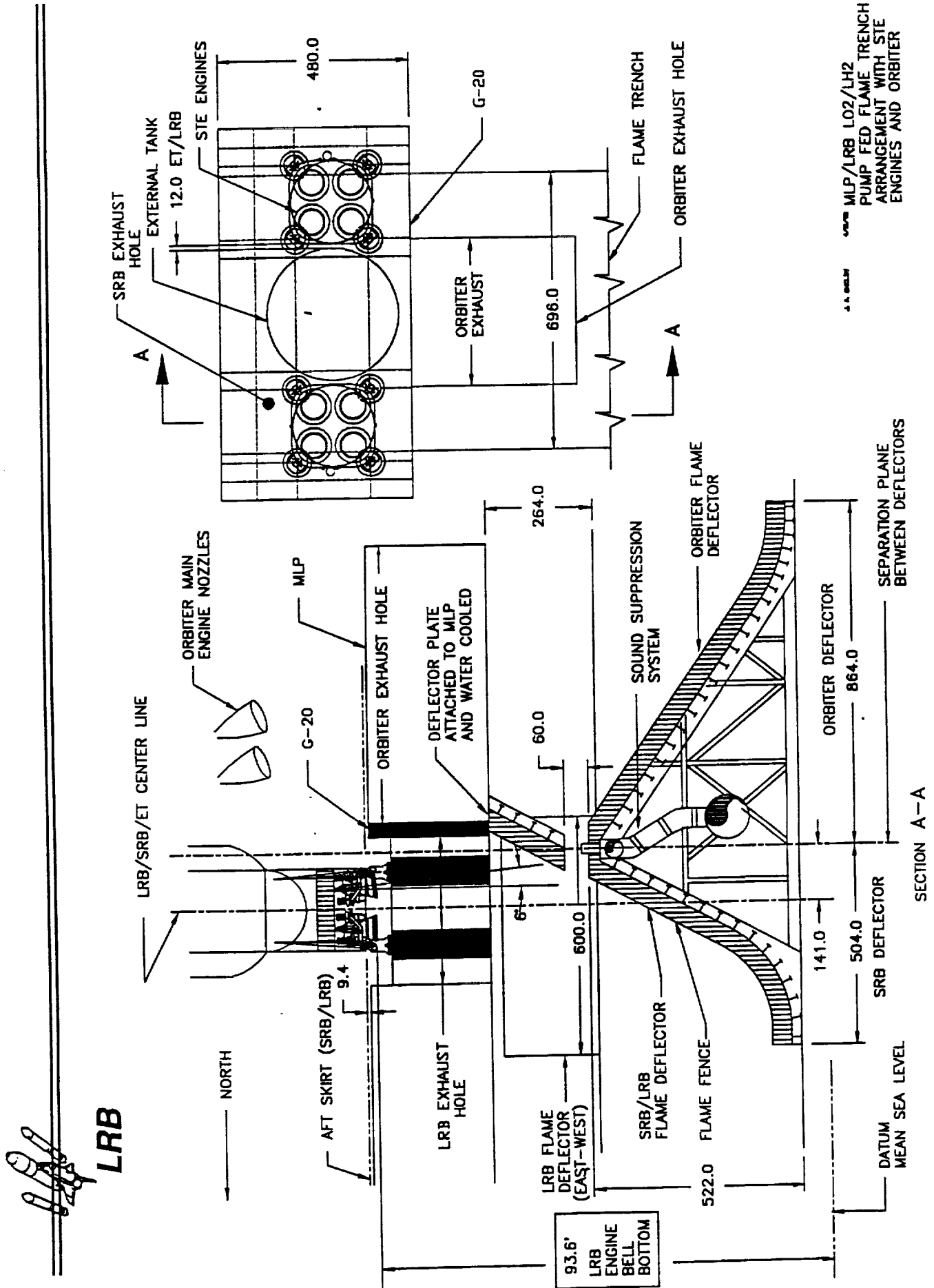
TOTAL WEIGHT 591 lbs

FILL AND DRAIN SYSTEM

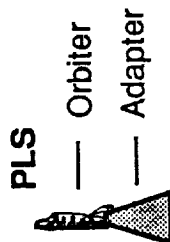
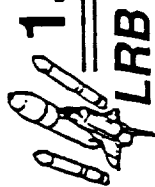
SAME AS ORBITER

LH2 261 lbs
LO2 242 lbs

TOTAL 503 lbs



1.5 STAGE PLS LAUNCH VEHICLE



LRB/PLS 1.5 STAGE VEHICLE

- Would not reach destination orbit of 50x100nm.
- Ascent Trajectory Simulation Aborted.

Gantry →

Crew, Bridge →

BASELINE LRB

50 FEET

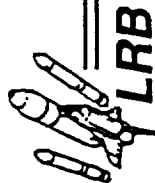
Performance Parameters at Termination of Simulation:

GLOW = 1,780 Klbs
H2 Weight = 225 Klbs
O2 Weight = 1,348 Klbs
Qty STEs = 4, drop 2
LV Length = 356.7 ft.
LV Diameter = 17.4 ft.
PL to 50x100 = 0

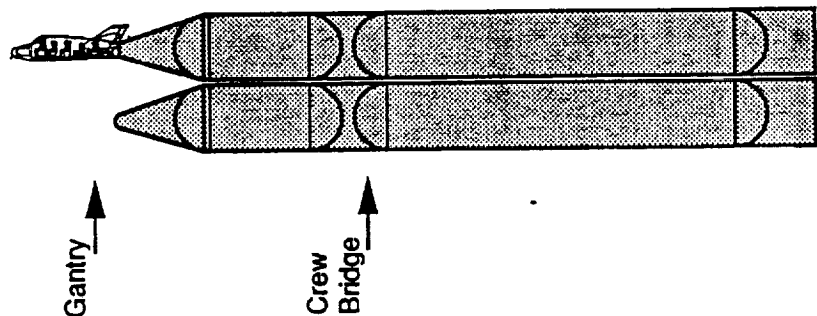
1.5 LRB MFrac = 0.88
Atlas MFrac = ~0.95

1.5 STAGE LRB IS INCAPABLE OF DELIVERING PLS TO LEO DUE TO LRB/STS WEIGHT REQUIREMENTS

PARALLEL PLS LAUNCH VEHICLE



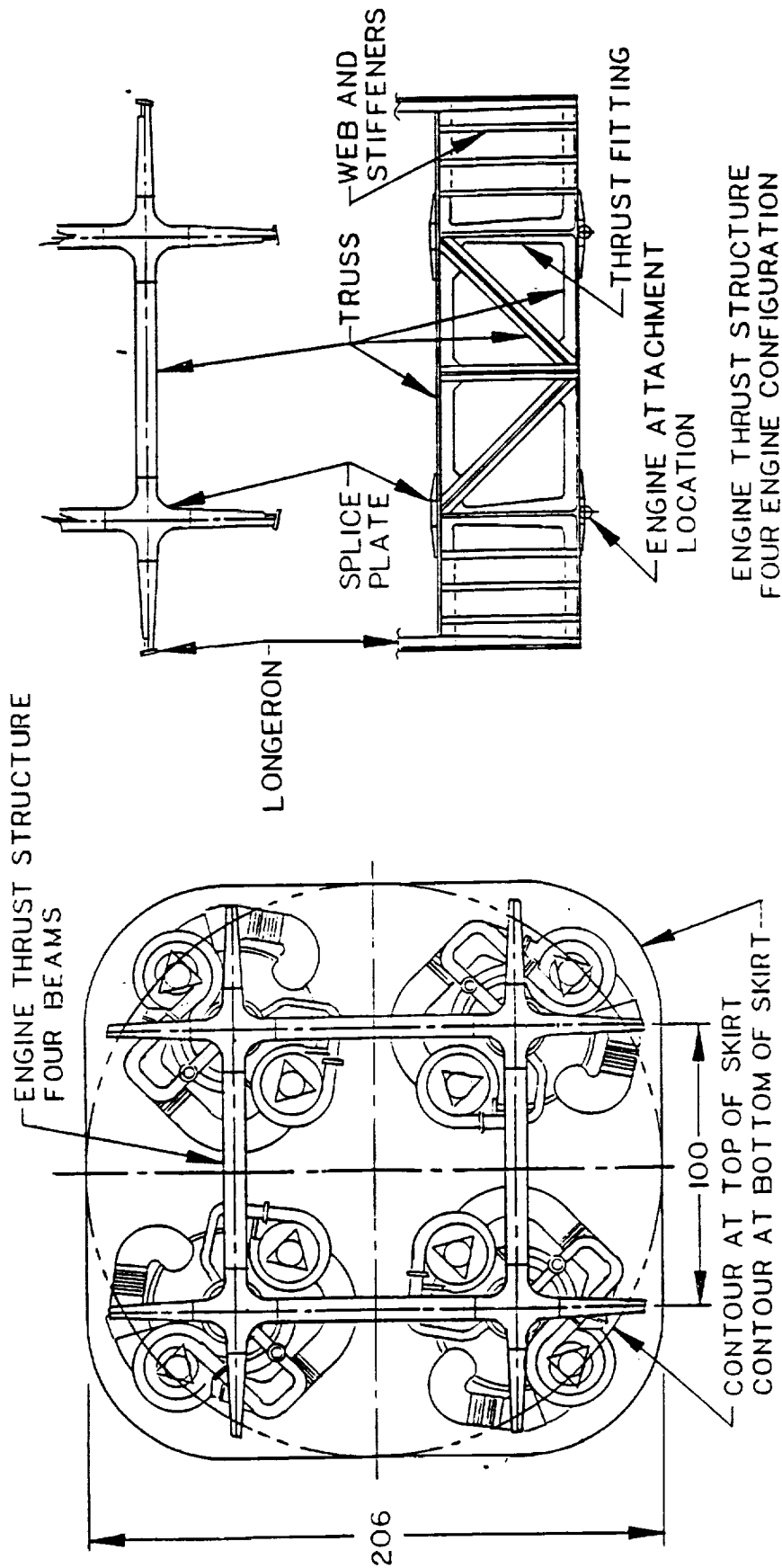
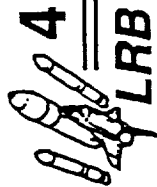
- Minimum Modifications to STS - LRB = ☐
- Simulations performed with 1 Core engine out



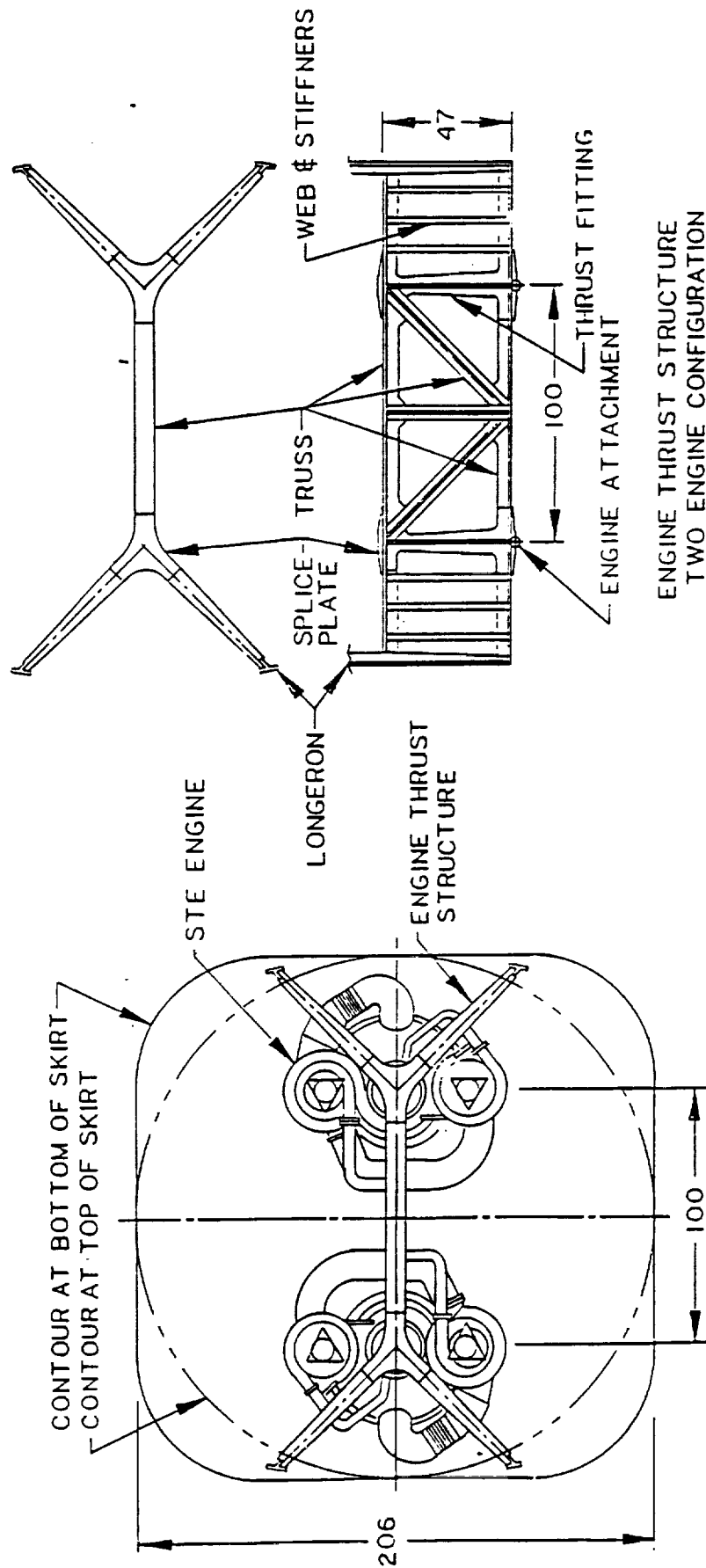
Vehicle Parameters	50 x 100 nm		SSF Transfer	
	LRB min mod	Optimized from LRB	LRB min mod	Optimized from LRB
Payload (Klbs)	53.5	33.3	49.4	33.3
Booster Inert Weight (Klbs)	123.1	112.6	123.1	114.7
Ascent Propellant (Klbs)	665.6	531.5	665.6	558.0
Upper Stage Inert Weight* (Klbs)	95.8	88.8	95.8	90.9
Ascent Propellant (Klbs)	665.6	531.5	665.6	558.0
GLOW (Klbs)	1,603.7	1,297.7	1,599.6	1,355.0
Vehicle Length (ft)	211	185	211	190
Vehicle Diameter (ft)	17.15	17.15	17.15	17.15
Qty Booster Engines (STE-20)	4	4	4	4
Lowest Throttle Setting	75%	75%	75%	75%
Qty Core Engines (STE-20)	2	2	2	2
Lowest Throttle Setting	75%	75%	75%	75%

*Upper stage inert weight includes: dry weight + residuals + FPR

LRB SQUARE SKIRT 4 - STE ENGINE CONFIGURATION

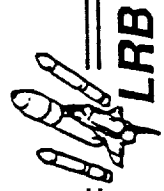


LRB SQUARE SKIRT 2 - STE ENGINE CONFIGURATION

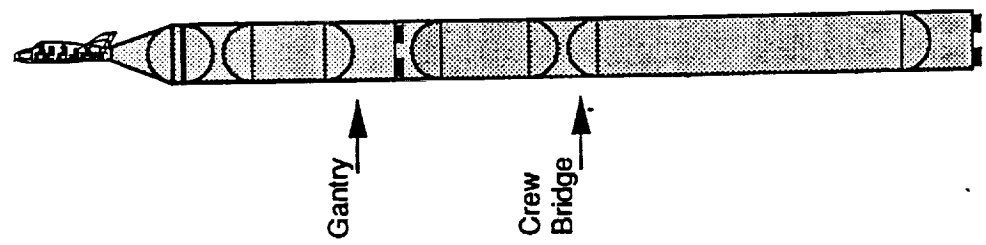


VIEW LOOKING DOWN (AFT) AT ENGINES

2 STAGE PLS LAUNCH VEHICLE 2-STE "LRB" UPPER STAGE



- Payload Delivered = 33,287 lbs; PLS Orbiter and Adapter
- Minimum Modifications to STS - LRB = ☐



Vehicle Parameters	50 x 100 nm			SSF Transfer			220 x 220		
	LRB min mod	Optimized from LRB	LRB min mod	LRB min mod	Optimized from LRB	LRB min mod	LRB min mod	Optimized from LRB	Optimized from LRB
Booster Inert Weight (Klbs)	111.8	99.8	111.8	111.8	102.9	111.8	111.8	113.7	113.7
Ascent Propellant (Klbs)	665.6	592.5	665.6	665.6	632.9	665.6	665.6	645.9	645.9
Upper Stage Inert Weight* (Klbs)	60.0	62.6	62.3	62.3	62.7	71.3	71.3	75.1	75.1
Ascent Propellant (Klbs)	223.2	256.2	252.3	252.3	257.5	285.4	285.4	330.3	330.3
GLOW (Klbs)	1,099.6	1,044.3	1,131.0	1,131.0	1,089.3	1,173.2	1,173.2	1,198.3	1,198.3
Vehicle Length (ft)	286	277	292	292	285	300	300	305	305
Vehicle Diameter (ft)	17.15	17.15	17.15	17.15	17.15	17.15	17.15	17.15	17.15
Qty Booster Engines (STE-20)	4	3	4	4	3	4	4	4	4
Lowest Throttle Setting	59%	75%	63%	63%	75%	75%	75%	75%	75%
Qty Upper Stage Engines (STE-20)	2	2	2	2	2	2	2	2	2
Lowest Throttle Setting	25%	26%	26%	26%	26%	28%	28%	30%	30%

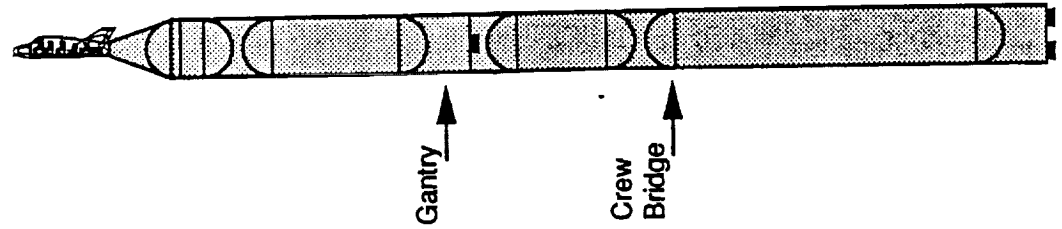
*Upper stage inert weight includes: dry weight + residuals + FPR + **restart + deorbit**
220x220 only

2 STAGE PLS LAUNCH VEHICLE 1-STE "LRB" UPPER STAGE



LRB

- Payload Delivered = 33,287 lbs; PLS Orbiter and Adapter
- Minimum Modifications to STS - LRB = ☐



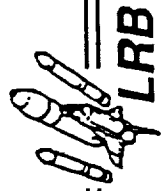
SSF Transfer 220 x 220

50 x 100 nm

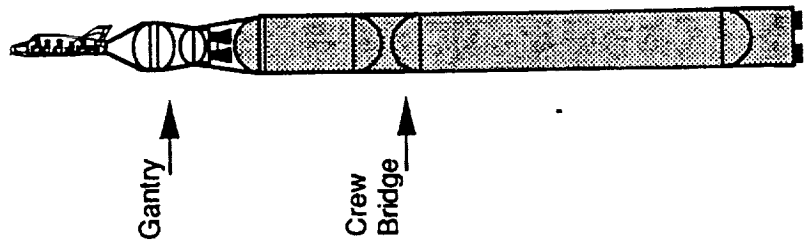
Vehicle Parameters	50 x 100 nm		SSF Transfer		220 x 220	
	LRB min mod	Optimized from LRB	LRB min mod	Optimized from LRB	LRB min mod	Optimized from LRB
Booster Inert Weight (Klbs)	111.8	95.6	111.8	97.6	111.8	113.7
Ascent Propellant (Klbs)	665.6	539.1	665.6	564.7	665.6	645.9
Upper Stage Inert Weight* (Klbs)	62.7	50.6	65.9	50.8	75.9	75.1
Ascent Propellant (Klbs)	242.7	212.3	282.1	215.0	326.2	330.3
GLOW (Klbs)	1,121.8	930.9	1,164.4	961.4	1,218.5	1,198.3
Vehicle Length (ft)	308	258	316	264	326	285
Vehicle Diameter (ft)	17.15	17.15	17.15	17.15	17.15	17.15
Qty Booster Engines (STE-20)	4	3	4	3	4	4
Lowest Throttle Setting	62%	75%	67%	75%	75%	75%
Qty Upper Stage Engines (STE-20)	1	1	1	1	1	1
Lowest Throttle Setting	52%	45%	53%	45%	59%	30%

*Upper stage inert weight includes: dry weight + residuals + FPR + **restart + deorbit**
220x220 only

2 STAGE PLS LAUNCH VEHICLE CENTAUR UPPER STAGE



- Payload Delivered = 33,287 lbs; PLS Orbiter and Adapter
- Minimum Modifications to STS - LRB = ☐
- Centaur sized for Payload Requirements (man-rated)



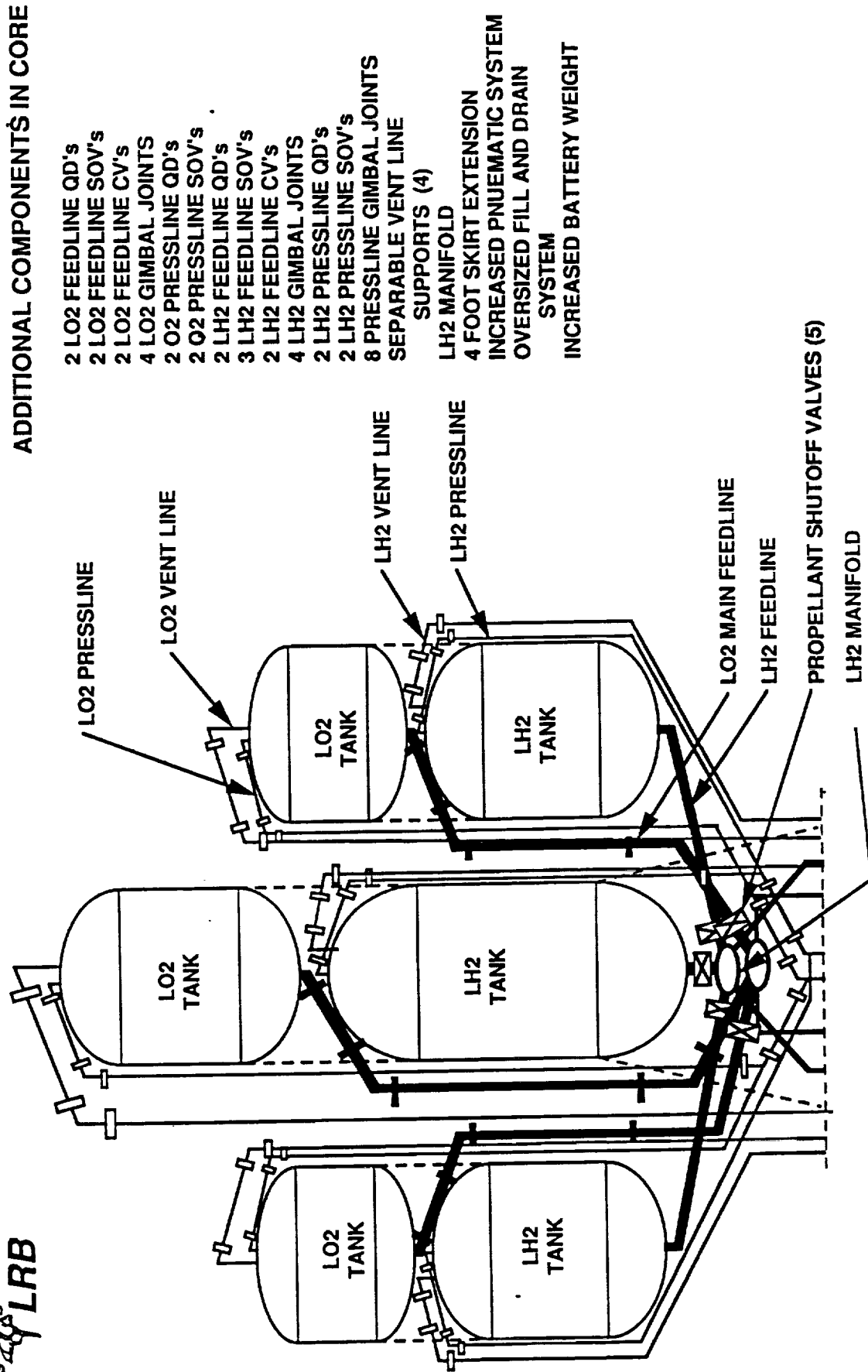
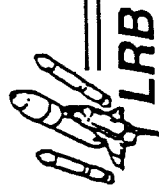
SSF Transfer 220 x 220

50 x 100 nm

Vehicle Parameters	50 x 100 nm		SSF Transfer		220 x 220	
	LRB min mod	Optimized from LRB	LRB min mod	Optimized from LRB	LRB min mod	Optimized from LRB
Booster Inert Weight (Klbs)	111.8	95.1	111.8	96.4	111.8	101.3
Ascent Propellant (Klbs)	665.6	533.4	665.6	548.9	665.6	611.7
Upper Stage Inert Weight* (Klbs)	8.3	9.3	8.4	9.3	10.1	10.1
Ascent Propellant (Klbs)	36.2	58.2	38.7	57.4	47.2	48.4
GLOW (Klbs)	861.0	729.3	863.6	745.2	873.7	804.8
Vehicle Length (ft)	235	212	236	215	239	225
Vehicle Diameter (ft)	17.15	17.15	17.15	17.15	17.15	17.15
Qty Booster Engines (STE-20)	4	3	4	3	4	3
Lowest Throttle Setting	26%	35%	26%	35%	27%	35%
Qty Upper Stage Engines (RL10-A4)	2	2	2	2	2	2
Lowest Throttle Setting	100%	100%	100%	100%	100%	100%

*Upper stage inert weight includes: dry weight + residuals + FPR + **restart + deorbit**
220x220 only

2 DROP TANK LRB PIPING SKETCH



ADDITIONAL COMPONENTS IN CORE

- 2 LO2 FEEDLINE QD's
- 2 LO2 FEEDLINE SOV's
- 2 LO2 FEEDLINE CV's
- 4 LO2 GIMBAL JOINTS
- 2 O2 PRESSLINE QD's
- 2 O2 PRESSLINE SOV's
- 2 LH2 FEEDLINE QD's
- 3 LH2 FEEDLINE SOV's
- 2 LH2 FEEDLINE CV's
- 4 LH2 GIMBAL JOINTS
- 2 LH2 PRESSLINE QD's
- 2 LH2 PRESSLINE SOV's
- 8 PRESSLINE GIMBAL JOINTS
- SEPARABLE VENT LINE
- SUPPORTS (4)
- LH2 MANIFOLD
- 4 FOOT SKIRT EXTENSION
- INCREASED PNEUMATIC SYSTEM
- OVERSIZED FILL AND DRAIN SYSTEM
- INCREASED BATTERY WEIGHT

PLS LV

CONCEPT TECHNICAL EVALUATIONS STATUS



LRB

RATING: 1 = low; 2 = mid; 3 = high

CONCEPT

RATING

REMARKS

• 1 1/2 Stage

2

Unable to achieve orbit; Mass Fraction too low;
may work if unconstrained

• Parallel

3

Offers most commonality, fits PAD tower
best for man ingress/egress, STE throttling
req'd within current range

• 2 Stage

- LRB Type Upper Stage W/1 Eng

2

Greatest commonality of 2 Stg concepts, high
2nd Stage throttling req'd

- LRB Type Upper Stage W/2 Eng.

1

2 STEs on 2nd Stage too much, very high
Throttling req'd

- Centaur Type Upper Stage

3

Shortest and lightest of 2 Stage concepts,
high throttling req'd on 3 & 4 STE Boosters,
2 STE Booster probably better option

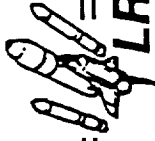
NOTE: PLS above Gantry for all 2 Stage options

• Drop Tanks

1

Plumbing too complex, no advantages over Parallel

FINDINGS AND RECOMMENDATIONS



LRB

FINDINGS TO-DATE

CONCEPT ITEMS

A. Parallel

ATTRIBUTES

- Most common to LRB
- Least PAD Tower Impact
- within STE throttle (75%)

CONCERNS

- Involves 2 LRBs

B. 2 Stage W/1 Eng
LRB US

- Uses LRB components

- High STE throttle (2 engine
Booster will reduce)
- PAD Tower Impact

C. 2 stage W/Centaur

- Shorter & lighter 2 Stage

- High STE throttle (2 engine
Booster will reduce)
- PAD Tower Impact

D. 1 1/2 Stage

- Simplified Concept

- STS Constraints Effect Wts.

E. Both 2 Stage W/2Engines
& Drop Tanks

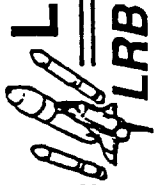
- None

- Not Practical

RECOMMENDATIONS FOR REMAINING MOD 10 EFFORTS

- Cease further work on Concepts in Item E.
- Continue further design studies on Concepts in Items A, B, C & D
- Refine concepts with size and structures unconstrained by STS, as required
- Provide cost analyses

LRB BOATTAIL FOR SHUTTLE-C APPLICATION

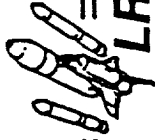


OBJECTIVE:

Develop a Conceptual Design To Determine The
Feasibility Of Utilizing The LRB Boattail (Aft Skirt)
For Shuttle-C Application

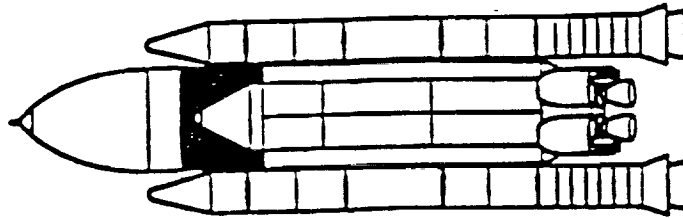
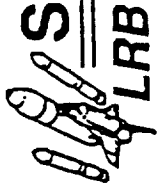
ASSUMPTIONS & GROUNDRULES

CONCEPT DESIGN-LRB BOATTAIL FOR SHUTTLE-C

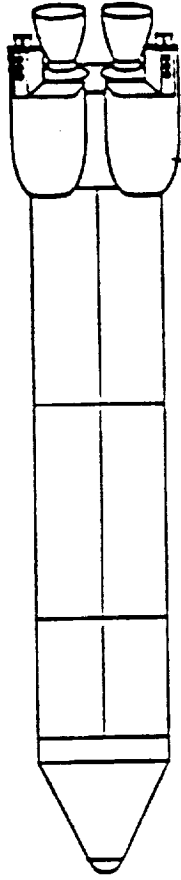
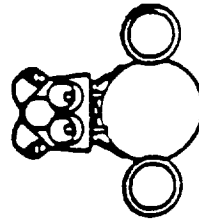


- Maximized use of STS-C boattail subsystems shall be made
- No impact to ET, ET Aft Attach Provisions, Cargo Carrier, Flame Trench, and only minor mods to other subsystems and GSE
- The baseline STE shall be used without mods except to the nozzle expansion ratio
- The Shuttle-C LRB boattail conceptual design shall be the 2-STE configuration
- The STS 3-g load factor limit shall apply to the LRB configured Shuttle-C
- LRB boattail STEs shall have same thrust vector angle as the STS-C boattail SSMEs
- The SRBs are replaced by LRBs on Shuttle-C with an LRB Boattail

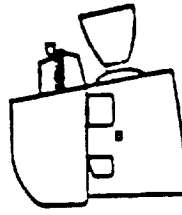
SHUTTLE-C CARGO ELEMENT (CE) SUB-ELEMENTS



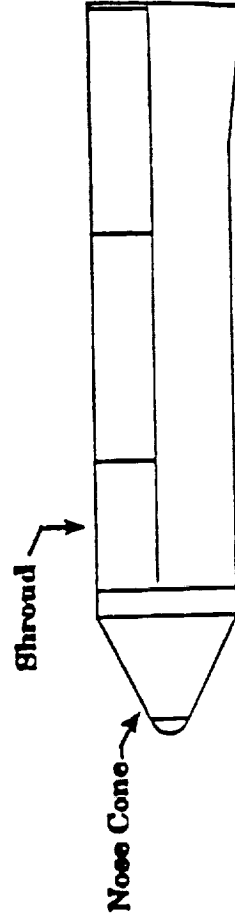
Shuttle-C (SH-C)



Cargo Element



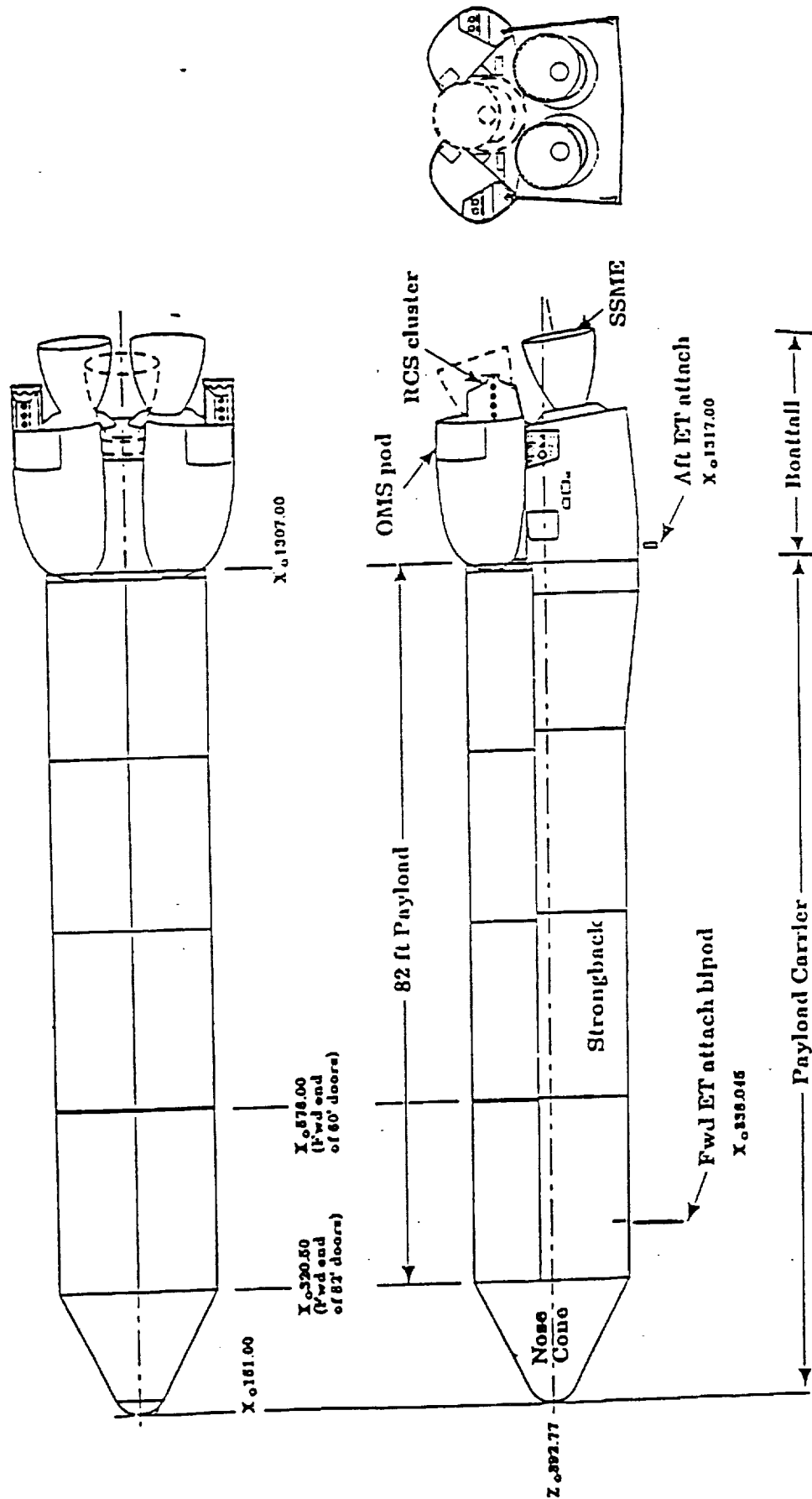
Boattail



Payload Carrier

REFERENCE SHUTTLE-C CARGO ELEMENT (CE)

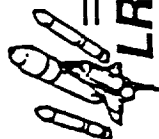
LRB



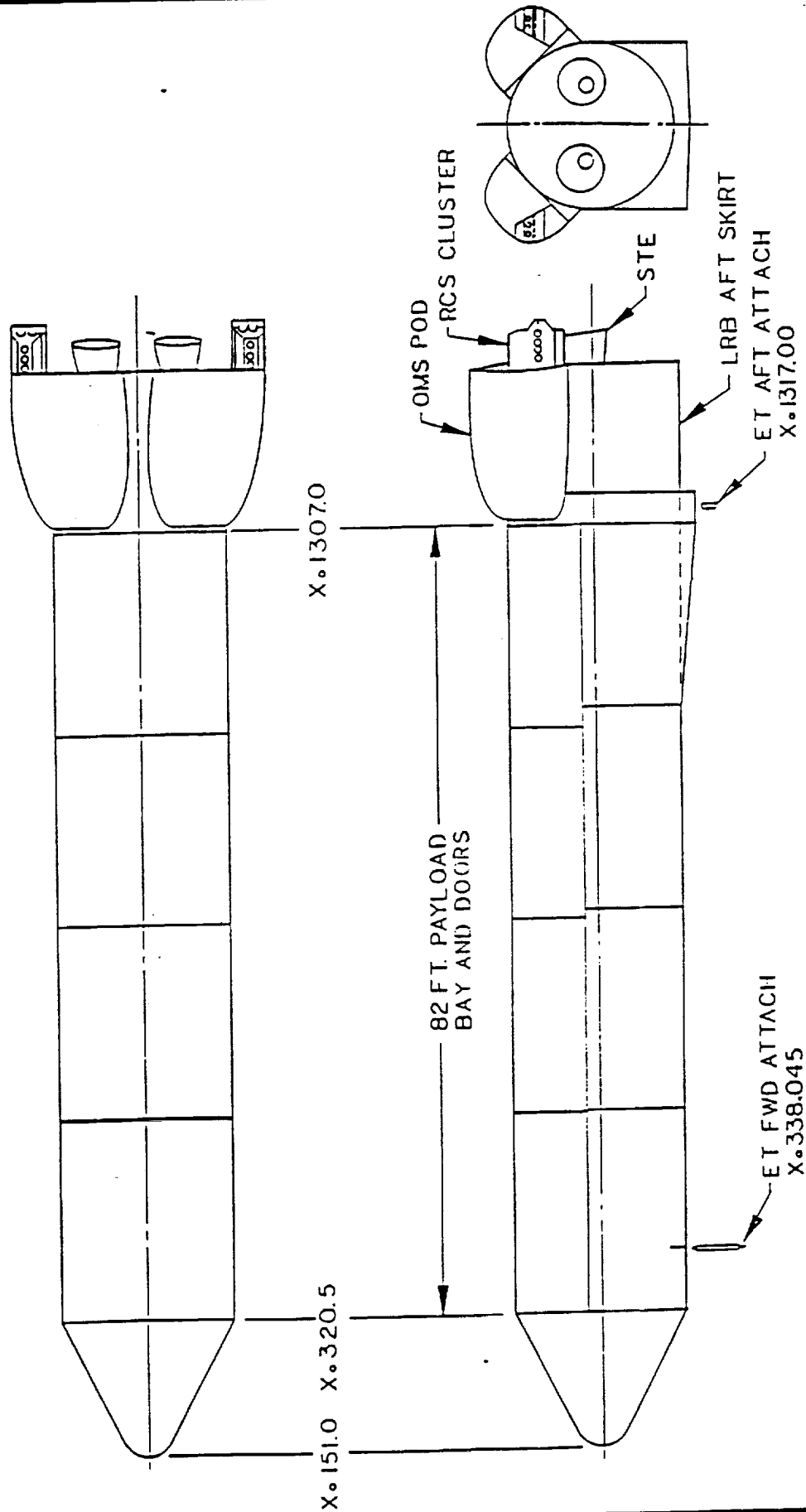
GENERAL DYNAMICS

Space Systems Division

LRB BOATTAIL ON SHUTTLE-C CARGO ELEMENT

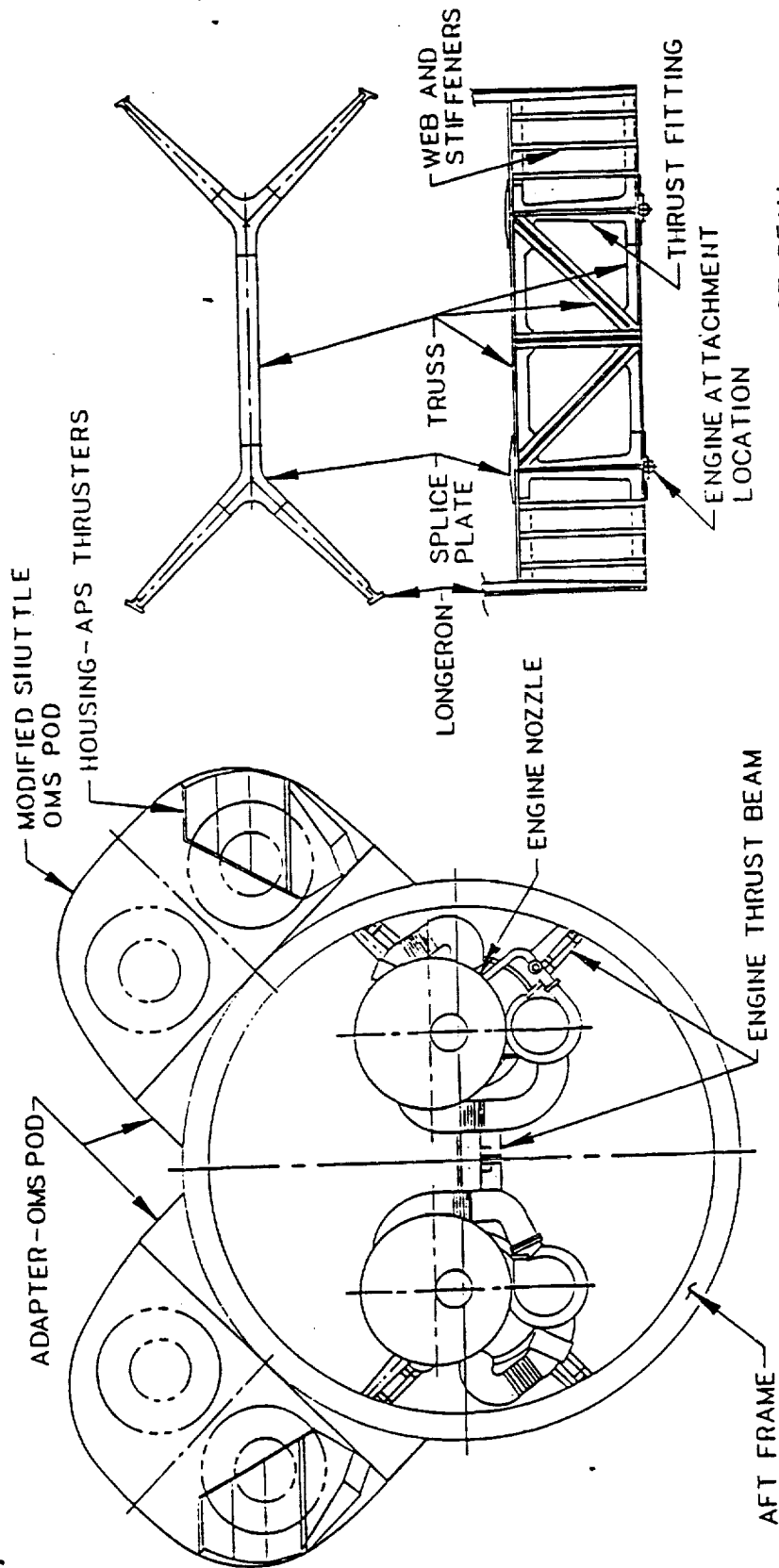


LRB



THRUST STRUCTURE FOR 2-STE LRB BOATTAIL

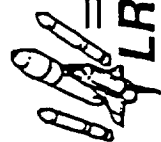
LRB



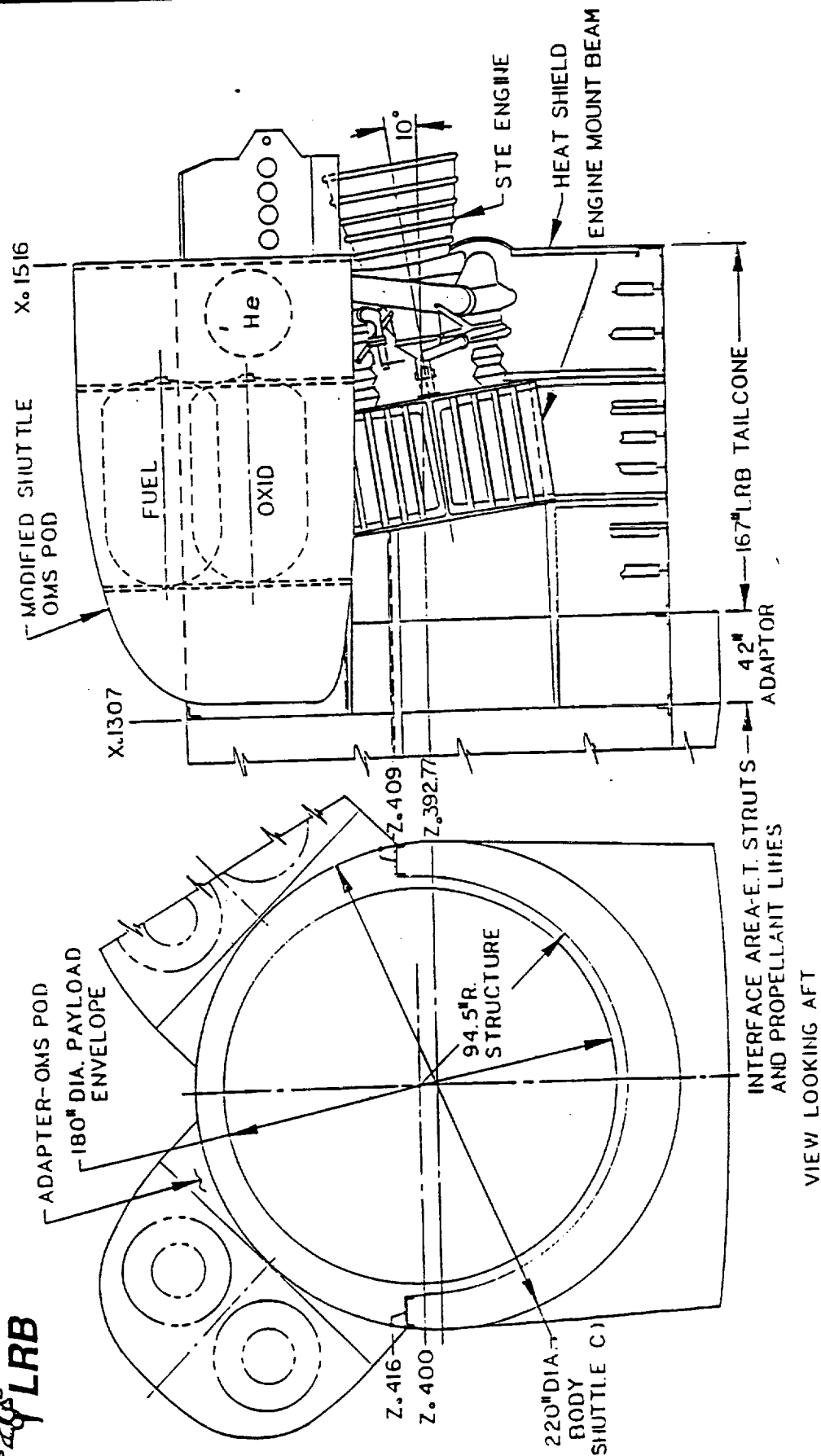
VIEW LOOKING FWD AT AFT END SHUTTLE C

THE PLS/LRB 2-STE OPTIMIZED THRUST STRUCTURE IS COMMON TO LRB BOATTAIL FOR STS-C

LRB BOATTAIL WITH SHUTTLE-C OMS PODS



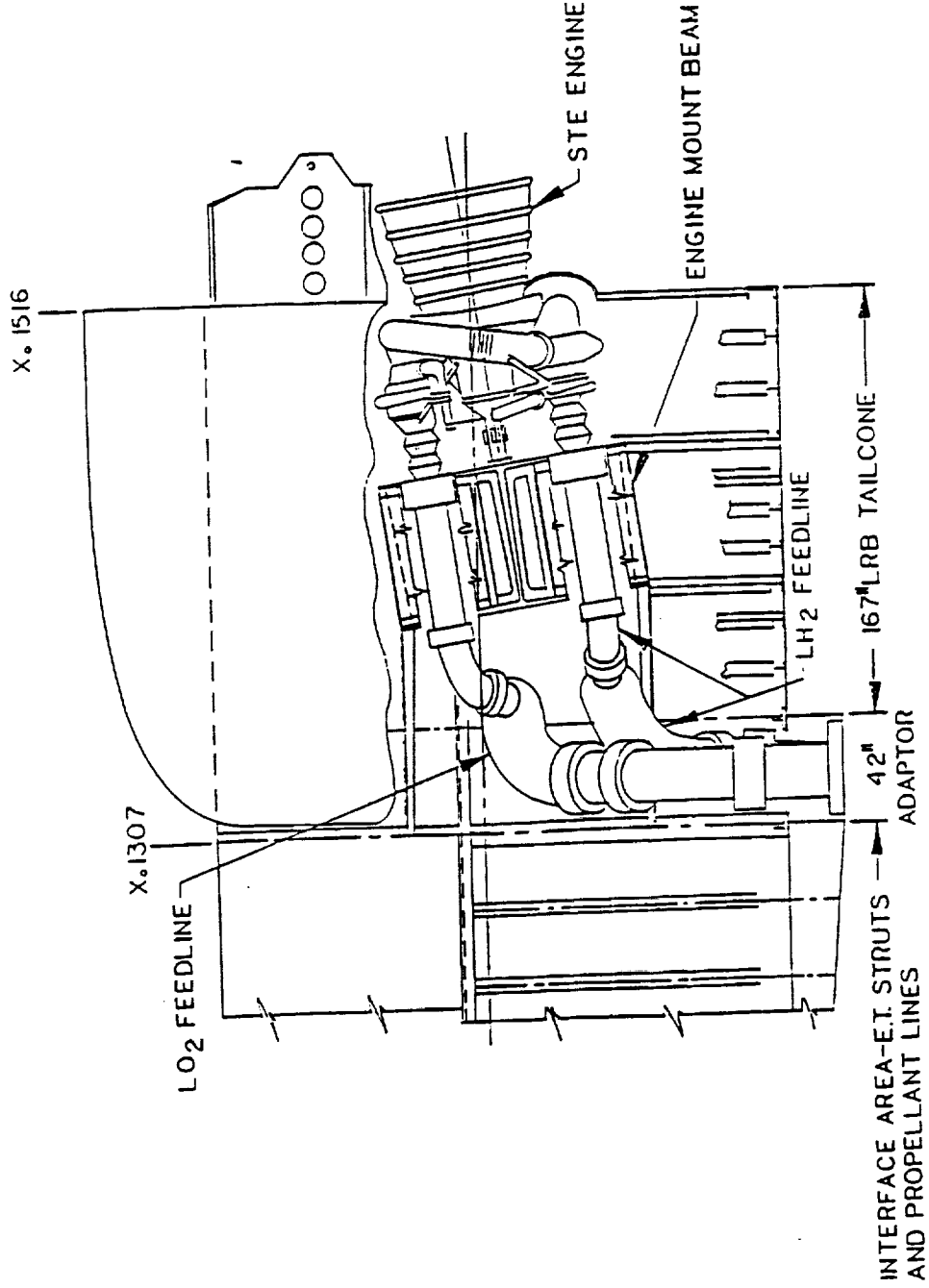
LRB



Interface Of Existing Flat Bottom STS Pod With Curved LRB Boattail Requires An Adapter

PROPELLANT FEED LINES OF STS-C LRB BOATTAIL

LRB



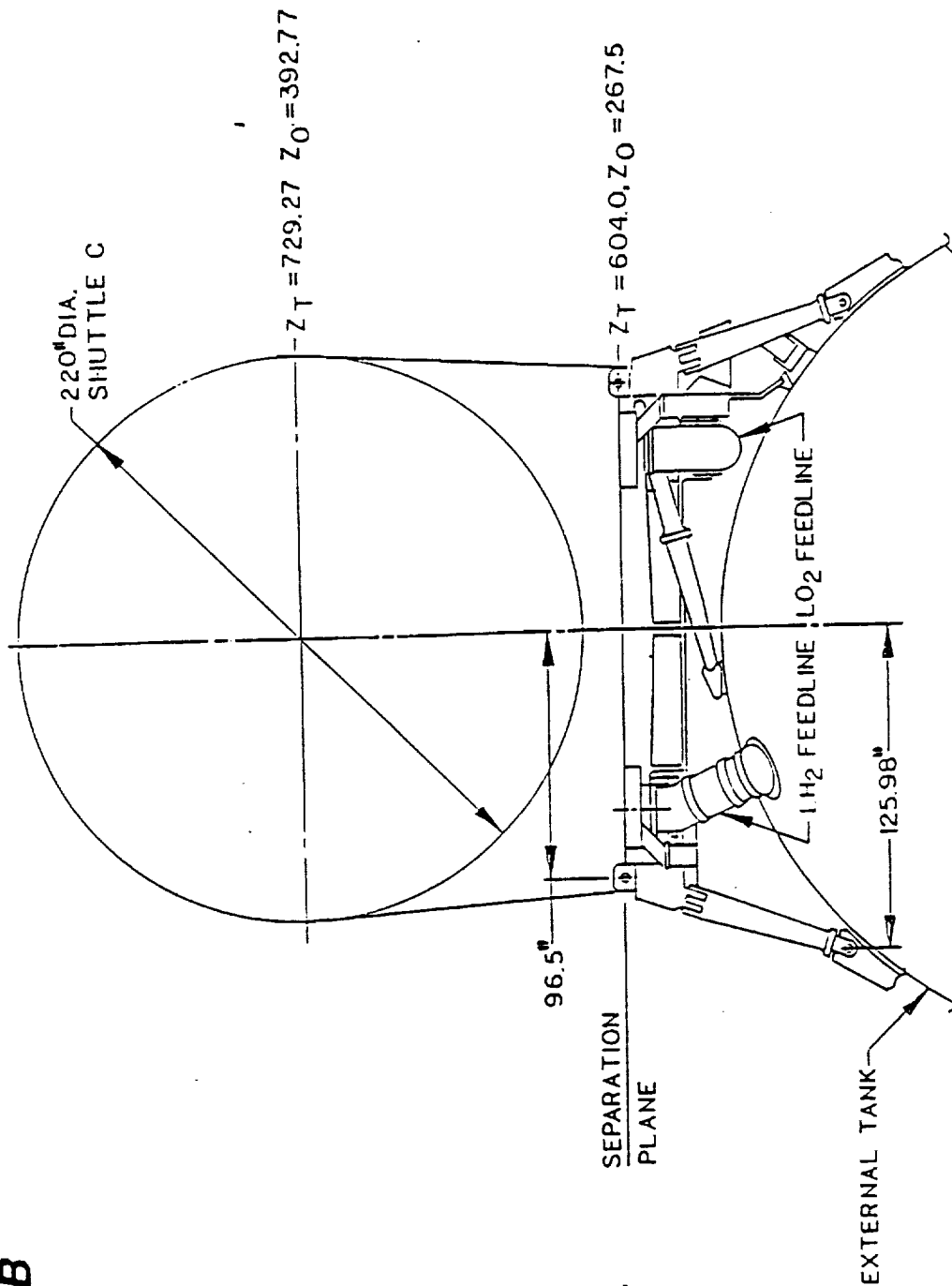
PROPELLANT LINES INTERFACE OF ET AND LRB BOATTAIL IDENTICAL TO STS

GENERAL DYNAMICS

Space Systems Division

STS ET AFT ATTACH I/F WITH LRB BOATTAIL

LRB



NO CHANGES REQUIRED TO STS ET AFT ATTACH SYSTEM FOR LRB BOATTAIL APPLICATION

SHUTTLE-C BOATTAIL WEIGHTS COMPARISON

LRB

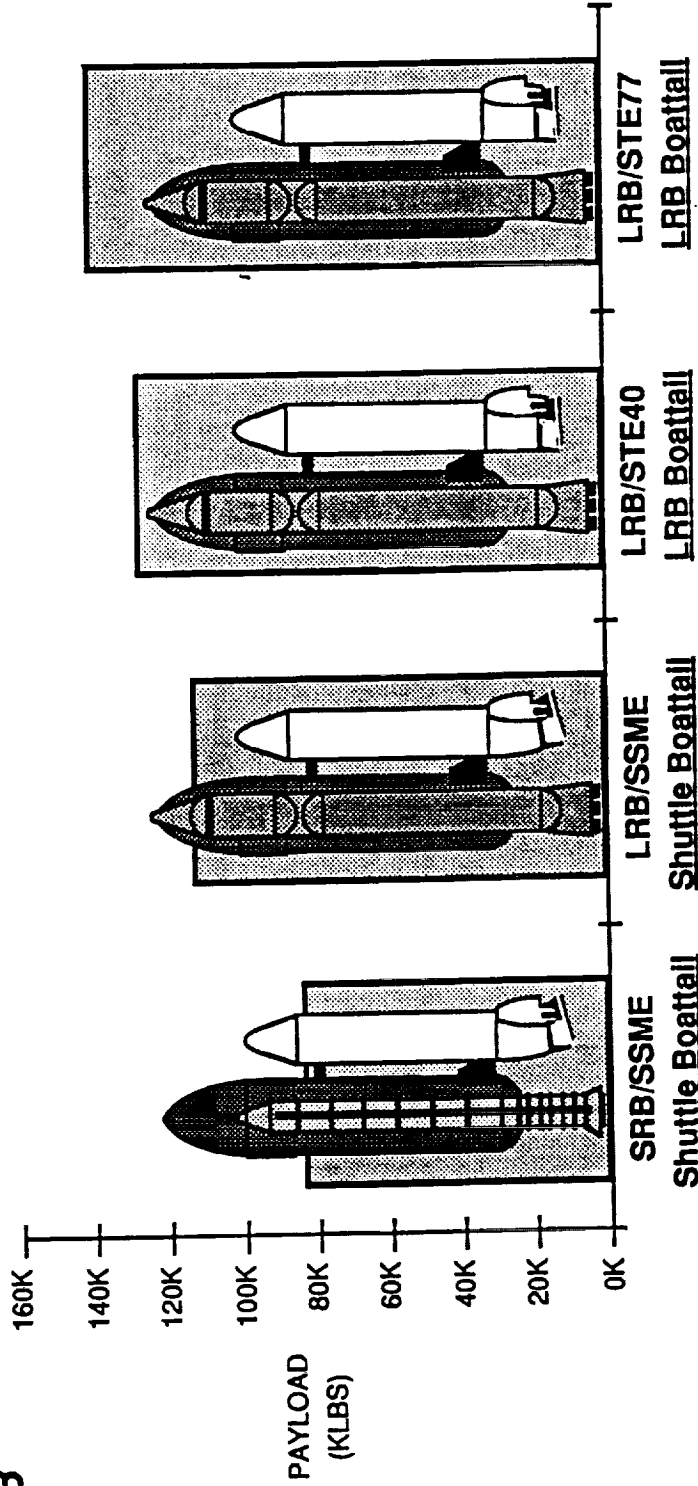
SUBSYSTEM / ITEM	STS-BOATTAIL / 2-SSME	LRB-BOATTAIL / 2-STE
DRY WEIGHT	46,115	40,896
STRUCTURE	14,127	13,181
BASIC SHELL STRUCTURE	6,474	7,355
THRUST STRUCTURE	3,702	1,905
OMS/RCS POD	3,031	3,031
SECONDARY STRUCTURE	920	890
ENVIRONMENTAL PROTECTION	2,483	2,012
THERMAL PROTECTION	624	341
BASE HEAT SHIELD	810	622
THERMAL CONTROL SYSTEM	661	661
PURGE & VENT SYSTEM	361	361
DRAIN/HAZARDOUS GAS DETECTION	27	27
AFT ET ATTACH ASSEMBLY	500	500
MAIN PROPULSION	21,206	18,735
MAIN ENGINES		
TVC	13,925	13,308
PROPELLANT SYSTEM	2,185	2,203
PNEUMATIC SYSTEM	4,352	2,479
PROPELLANT MNGMNT	706	706
AUXILIARY PROPULSION SYSTEM	38	38
ELECTRICAL PWR & DISTRIB	3,424	3,424
AVIONICS	1,583	1,583
HYDRAULIC PWR & DISTRIB	820	820
ENVIRONMENTAL CONTROL	1,330	0
	642	642

A 5 Klb Lighter And Simpler Structural Design Are Attributes Of An LRB vs An STS Boattail

SHUTTLE-C PERFORMANCE WITH LRB VS SRB



LRB



LRB CONFIGURED STS-C LAUNCH VEHICLES PROVIDE SIGNIFICANTLY HIGHER PAYLOAD CAPABILITY

FINDINGS

CONCEPT DESIGN-LRB BOATTAIL FOR SHUTTLE-C



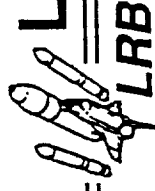
LRB

- A 69% increase in Shuttle-C payload performance possible with an LRB configured Shuttle-C that includes an LRB boattail Cargo Element (140,224 lb vs 83,140 lb)
- A 5000 lb weight reduction possible by replacing STS with an LRB boattail
- LRB and LRB boattail engine commonality simplifies Shuttle-C design
- A third engine can be integrated in the LRB boattail without major modification
- No problems expected in the integration of the OMS pods and the ET attach assembly based on conceptual layouts
- Cylindrical shaped LRB vs "breadloaf" shaped boattail simplifies design and makes possible Cargo Carrier segments commonality for significant fabrication cost savings

The many advantages of LRB/LRB boattail make it a viable candidate for Shuttle-C

RECOMMENDATIONS

LRB BOATTAIL FOR SHUTTLE-C APPLICATION

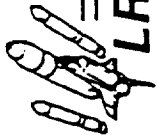


Continuation of Shuttle-C LRB BOATTAIL Study :

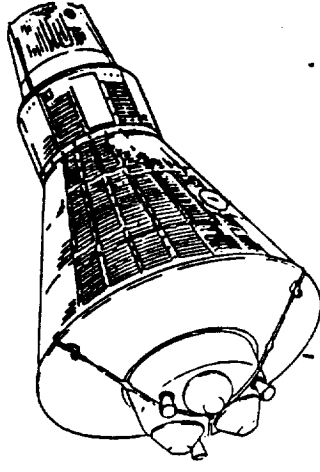
- Do feasibility study to develop a conceptual design of an LRB Boattail optimized APS Pod or integration of the APS components within the boattail structure as options to the present large/heavy STS OMS Pod.
- Extend the conceptual design to determine the feasibility/compatibility of integrating the Shuttle-C subsystems in the LRB Boattail that were not addressed in this phase, viz: Avionics; Electrical; ECS; etc.
- Develop a conceptual design of the 3-STE LRB Boattail configuration.
- Conduct performance analyses of following STS-C configurations:
 - Baseline LRBs with 3-STE40 LRB Boattail
 - Baseline LRBs with 3-STE77 LRB Boattail
 - ASRMs with 3-SSME STS Boattail
 - ASRMs with 3-STE77 LRB Boattail
 - ASRMs with 2-SSME STS Boattail
- Cost analysis of STS vs LRB Boattails for Shuttle-C application

MANNED TRANSPORTATION SYSTEMS

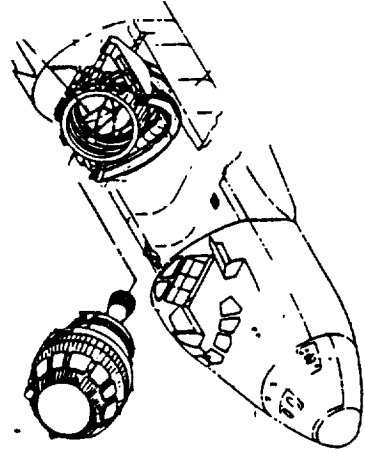
GENERAL DYNAMICS EXPERIENCE



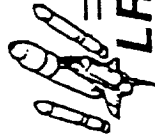
LRB



- ATLAS (RELIABLE) TO MERCURY-ATLAS (MAN-SAFE)
- SHUTTLE-CENTAUR TO TITAN-CENTAUR (FROM MANNED UPPER STAGE TO UNMANNED UPPER STAGE)



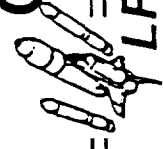
BASIC PRINCIPLES ON MERCURY-ATLAS PROGRAM



LRB

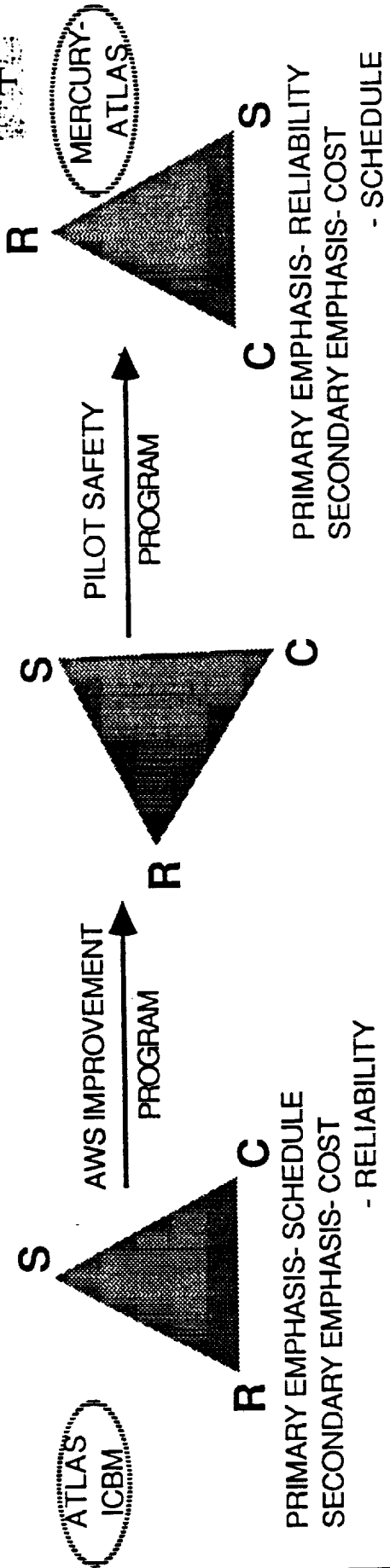
- MINIMUM OF NEW DEVELOPMENTS
 - NO CHANGE TO BOOSTER VEHICLE
- PILOT SAFETY PROGRAM
 - ENHANCE SYSTEM RELIABILITY
 - ESCAPE SYSTEM TO FILL GAP BETWEEN 100% RELIABILITY AND BOOSTER RELIABILITY

CHANGE IN PROGRAM MANAGEMENT EMPHASIS



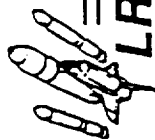
LRB

PHASE-IN OF PILOT SAFETY PROGRAM



RESULTS:

- 1) ENGINE DEMONSTRATED RELIABILITY SUBSTANTIALLY ENHANCED (THROUGH TESTING AND TIGHTENING OF QUALITY CONTROL)
- 2) ATLAS ICBM RELIABILITY SIGNIFICANTLY INCREASED
- 3) 100% SUCCESSFUL MANNED FLIGHTS WITH ATLAS



LRB

PILOT SAFETY PROGRAM

GENERAL DYNAMICS
Space Systems Division

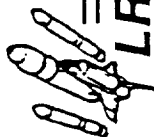
PILOT SAFETY PROGRAM

8. SPECIAL FAILURE ANALYSIS
7. SPECIAL HANDLING PROCEDURES
6. REVIEW OF ALL PREVIOUS TEST DATA
5. COMPONENT RELIABILITY DEMONSTRATION
4. SPECIAL QUALITY-ASSURANCE PLAN
3. SPECIAL DESIGN FEATURES
2. PERSONNEL
1. TEAMWORK

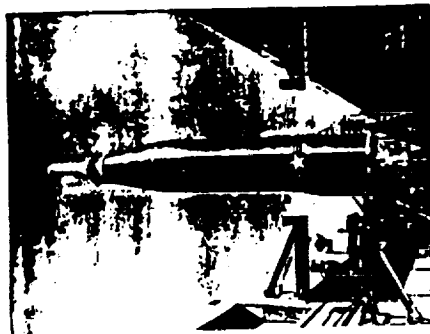
ATLAS EXPERIENCE

ORIGINAL PAGE IS
OF POOR QUALITY

MISSILE TO MAN-SAFE SYSTEM



LRB



ATLAS MISSILE



MERCURY-ATLAS

ORIGINAL PAGE IS
OF POOR QUALITY

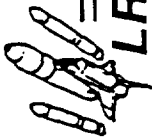
MAJOR CHANGES FROM MISSILE TO MERCURY-ATLAS	DESCRIPTION
• ENHANCE RELIABILITY	• SYSTEM COMPONENTS HAND PICKED TO HAVE CLOSE TO SPEC VALUES
• ADDITION OF ASIS (ABORT SENSING & INSTRUMENTATION SYSTEM)	• NUMBER OF INSTRUMENTATION & LOGIC SYSTEMS TO SENSE HAZARDS, ABNORMAL ENGINE OPERATION, SPURIOUS SIGNAL TO THE RSS ESCAPE SYSTEM
• ESCAPE SYSTEM	• CAPSULE EJECTED TO PROVIDE SAFE ESCAPE FROM IMPENDING FAILURE

GROUND RULES FOR SHUTTLE-CENTAUR

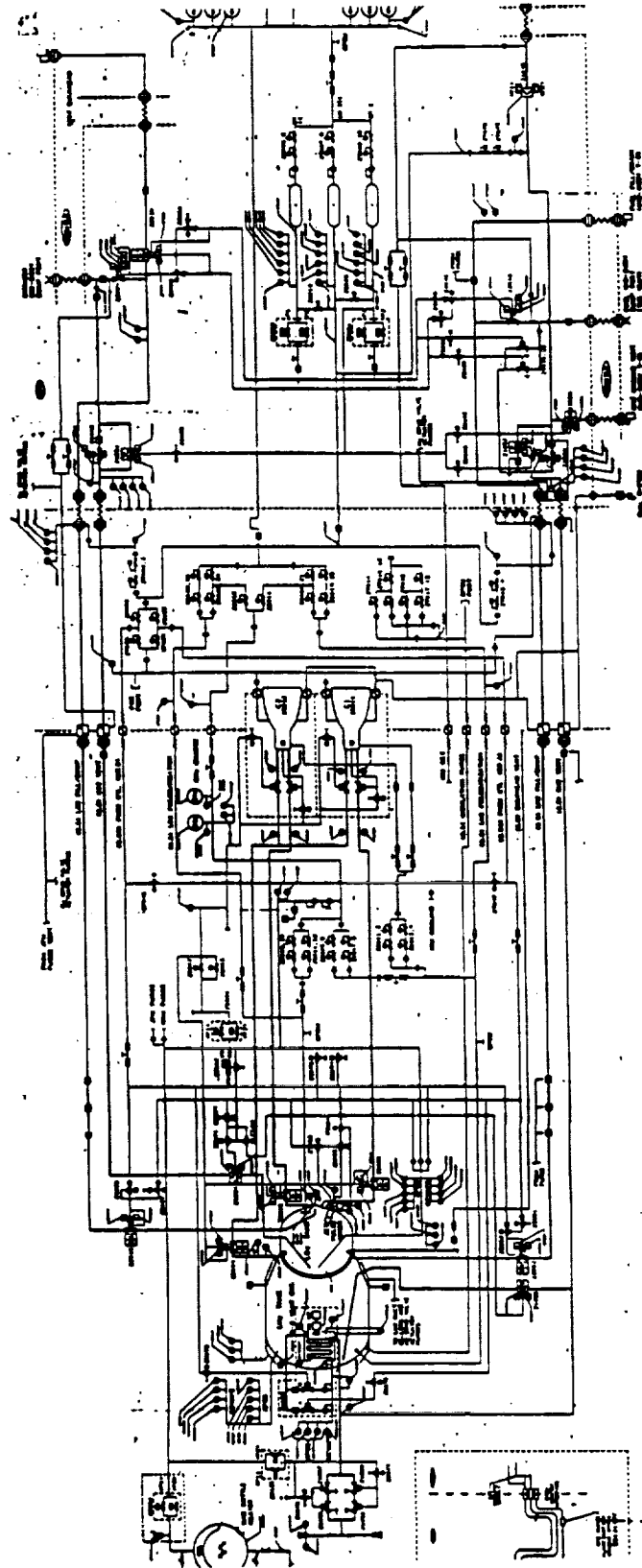


- CARGO P/L RULES OR LAUNCH SYSTEM RULES?
 - INITIALLY ONLY MINOR MODS EXPECTED
 - LOTS OF CONFUSION
 - UNIQUE MISSION REQUIREMENTS
- FAIL OPERATIONAL FAIL SAFE
 - PRESSURIZATION, VENTING, AVIONICS,
- PROPELLANT DUMP SYSTEM FOR ABORT
- ALMOST AUTONOMOUS SYSTEM
 - ASTRONAUT INITIATE ABORT DUMP SEQUENCE & P/L RELEASE

SHUTTLE-CENTAUR FLUIDS SCHEMATIC



LRB



SOLENOID VALVES

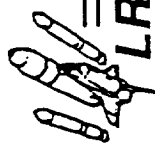
44 PILOT OPERATED
34 SOLENOID VALVES
29 CHECK VALVES
26 CRYO VALVES
5 PRESSURE REGULATORS

138

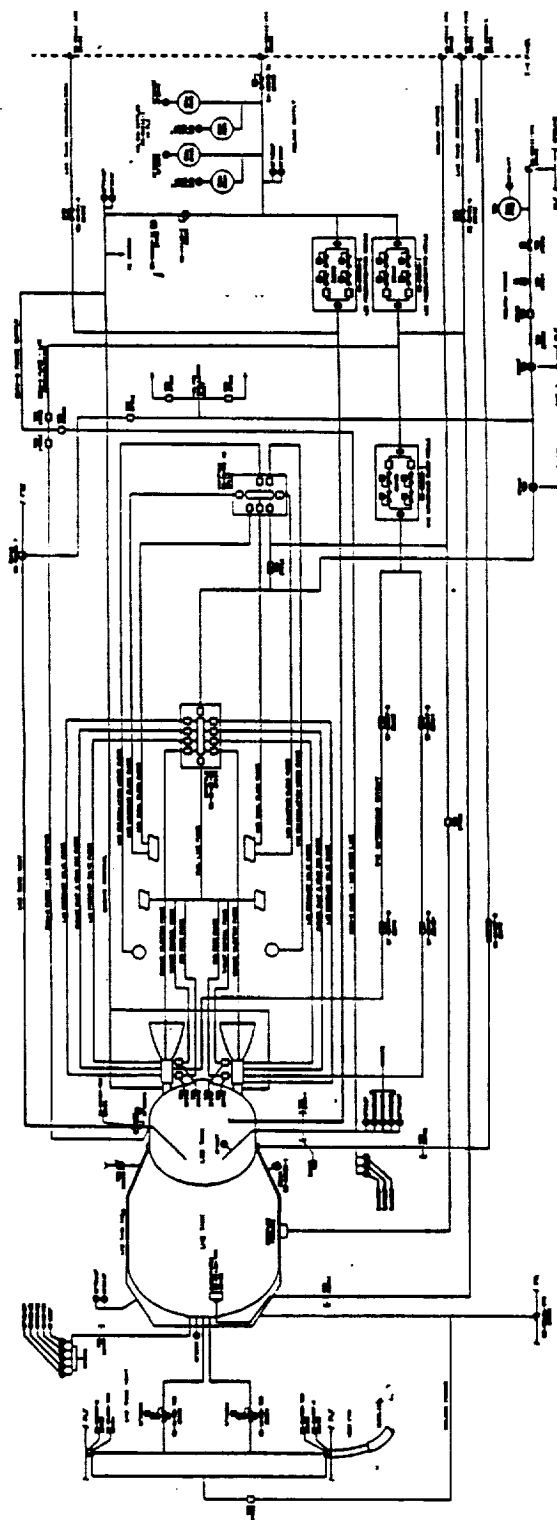
22 HELIUM BOTTLES
1 N₂H₄ BOTTLE

ORIGINAL PAGE IS
OF POOR QUALITY

TITAN-CENTAUR FLUIDS SCHEMATIC



LRB

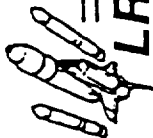


13	PILOT OPERATED	SOLENOID VALVES
1	SOLENOID VALVE	
6	CHECK VALVES	
7	CRYO VALVES	
1	PRESSURE REGULATOR	
		<hr/> 28

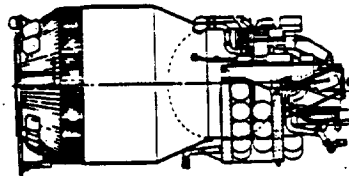
5 HELIUM BOTTLES
2 N₂H₄ BOTTLES

ORIGINAL PAGE IS
OF POOR QUALITY

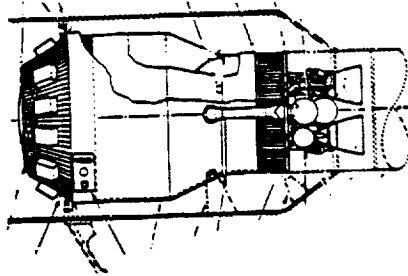
ELV UPPER STAGE TO SHUTTLE UPPER STAGE



LRB

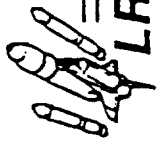


SHUTTLE-CENTAUR



TITAN-CENTAUR

MAJOR CHANGE FROM ELV TO SHUTTLE UPPER STAGE	DESCRIPTION
<ul style="list-style-type: none"> • SAFETY ENHANCEMENT - ADDITION OF DUMP SYSTEM & HDSS - HIGH DEGREE OF REDUNDANCY FAIL-OP FAIL SAFE 	<ul style="list-style-type: none"> • AS SHOWN IN SCHEMATIC, NUMBER OF EXTRA COMPONENTS WERE ADDED TO MAKE SYSTEM DUAL FAILURE TOLERANT, AND START DUMP SEQUENCE IN CASE OF ANY HAZARD
<ul style="list-style-type: none"> • LOT OF ANALYSIS 	<ul style="list-style-type: none"> • MORE FRACTURE CONTROL AND "WHAT IF" SCENARIO OF A MORE COMPLEX SYSTEM INVESTIGATED
<ul style="list-style-type: none"> • DISPLAY AND CONTROLS 	<ul style="list-style-type: none"> • SOME CRITICAL DISPLAYS AND DEGREE OF MANUAL CONTROL ON PROPELLANT DUMP PROVIDED
<ul style="list-style-type: none"> • RIGID QUALITY CONTROL MANAGEMENT REVIEW 	<ul style="list-style-type: none"> • NUMBER OF INTEGRATION PANELS, AND REVIEW COMMITTEES



LRB

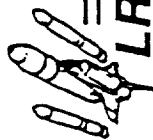
DESIGN GUIDELINE DOCUMENT

GENERAL DYNAMICS
Space Systems Division

1. JSC-23211, "GUIDELINES FOR MAN RATING SPACE SYSTEMS" (SEPTEMBER 1988)
2. JSCM-8080, "MANNED SPACECRAFT CRITERIA & STANDARDS" (MARCH 2, 1982 / CHANGE 10)
3. AFSC DH3-2, "DESIGN HANDBOOK, SERIES 3-0, SPACE AND MISSILE SYSTEMS" (MARCH 20, 1969)
4. KHB 1700.7, SPACE TRANSPORTATION SYSTEM PAYLOAD HANDBOOK
5. NHB 1700.7, SAFETY POLICY AND REQUIREMENTS
6. SSP 30000, SPACE STATION PROGRAM DEFINITION AND REQUIREMENTS
7. GDSS-ALS-RPT-89-011, "ALS ADAPTATION FOR MANNED CARGO" (SEPTEMBER 1989)

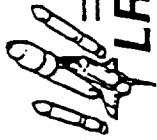
CLASSIFICATION OF SPACE SYSTEMS (JSC-23211)

GENERAL DYNAMICS
Space Systems Division

 LRB

SPACE SYSTEM	MISSION OBJECTIVE	ATTRIBUTES	EXAMPLES
MAN-RATED SYSTEM	MISSION SUCCESS & MISSION SAFETY EQUALLY IMPORTANT	<ul style="list-style-type: none"> HIGHEST POSSIBLE RELIABILITY FAIL SAFE OPERATION DESIGNED INTO TOTAL SYSTEM ESCAPE SYSTEM PROVIDES ULTIMATE BACK-UP 	<ul style="list-style-type: none"> SPACE STATION
HIGHLY RELIABLE	<ul style="list-style-type: none"> MISSION SUCCESS PRIMARY IMPORTANCE MISSION (OR CREW) SAFETY ENHANCED AS A BY PRODUCT 	<ul style="list-style-type: none"> HIGHEST POSSIBLE RELIABILITY FAIL SAFE OPERATION DESIGNED INTO TOTAL SYSTEM 	<ul style="list-style-type: none"> SHUTTLE - LRB APOLLO LUNAR LANDER PRECIOUS CARGO COMMERCIAL AIRLINES
MAN SAFE	<ul style="list-style-type: none"> MISSION (OR CREW) SAFETY HIGHER EMPHASIS THAN MISSION SUCCESS 	<ul style="list-style-type: none"> RELIABLE FAIL SAFE OPERATION ONLY OF ESCAPE SYSTEM 	<ul style="list-style-type: none"> CREW EMERGENCY RETURN VEHICLE (CERV) - LRB MERCURY SPACE PROGRAM FIGHTER AIRCRAFT
REPLACABLE	<ul style="list-style-type: none"> NOT VERY HIGH EMPHASIS ON MISSION SAFETY OR MISSION SUCCESS 	<ul style="list-style-type: none"> EMPHASIS ON COST, SCHEDULE, ETC. 	<ul style="list-style-type: none"> LOW VALUE CARGO (PROPELLANTS, RE-SUPPLY AND EXPENDABLES)

STRUCTURAL FACTORS OF SAFETY

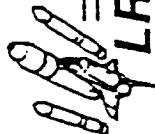


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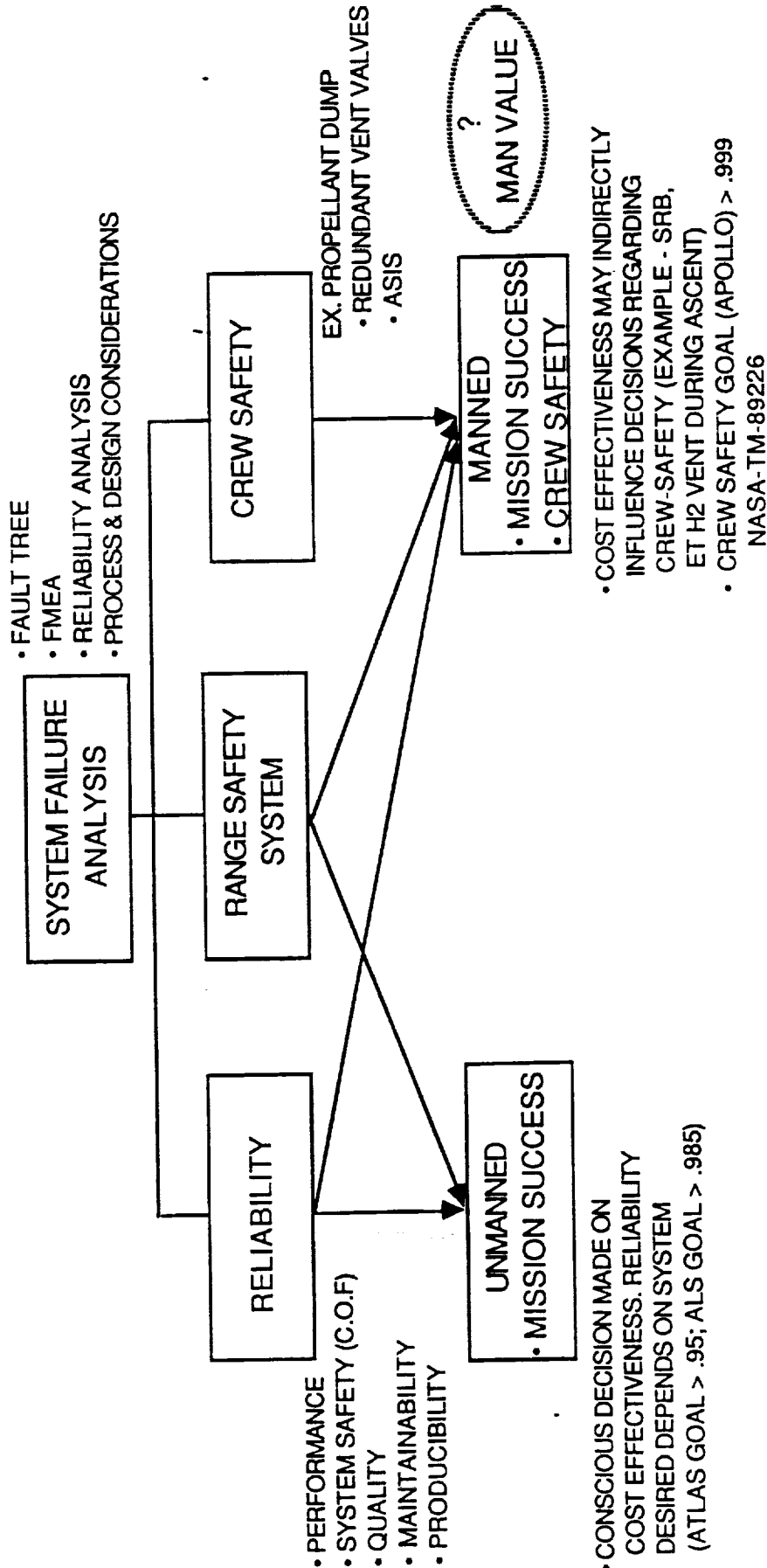
FACTOR LOADING SOURCE	AIRCRAFT	SHUTTLE ET	ATLAS
MECHANICAL LOADS			
YIELD	1.0	1.1	1.0
ULTIMATE	1.5	1.4*	1.25
UNREGULATED PRESSURE			
YIELD	1.0	1.1	1.0
ULTIMATE	1.5	1.4	1.25
BURST	2.0	1.4	1.25
REGULATED PRESSURE			
YIELD	1.0	1.1	1.0
ULTIMATE	1.5	1.25	1.25
BURST	2.0	1.25	1.25

* FOR WELL DEFINED LOADS, F.S. = 1.25 (MMC-ET-SE25-0, NAS8-303000)

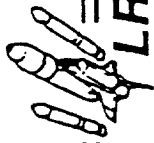
DIFFERENCES BETWEEN MANNED AND UNMANNED SYSTEM



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ATTRIBUTES OF MANNED AND UNMANNED SPACE SYSTEMS



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ATTRIBUTES OF HIGHLY RELIABLE UNMANNED SYSTEM

- PROVEN TECHNOLOGY AND WELL CHARACTERIZED MATERIAL
- FLY THROUGH FAILURES (CRITICAL SYSTEM EXCEPT STRUCTURES, PRESSURE VESSELS & THERMAL PROTECTION SYSTEM SHOULD BE DESIGNED WITH APPROPRIATE DEGREE OF FUNCTIONAL REDUNDANCY)
- ROBUST - A LOT OF MARGIN, SIMPLE DESIGN
- CONTROL OF FAILURE PROPAGATION (HDSS, IHM, LOW CORRELATION OF FAILURE ETC.)
- DEMONSTRATION & VERIFICATION OF RELIABILITY

ADDITIONAL ATTRIBUTES OF HIGHLY RELIABLE MANNED SYSTEM

- CREW DISPLAY AND POSSIBLE PROVISION FOR INTERVENTION (EXTRA REDUNDANCY BY CREW)
- EXTRA REDUNDANCY, DETECTION AND CONTROL WHICH ENHANCES CREW SAFETY AND SAFE ABORT CHANCES



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MANNED TRANSPORTATION SYSTEMS

PRELIMINARY CONCLUSIONS

- A HIGHLY RELIABLE SYSTEM IS ESSENTIAL FOR ALL SPACE SYSTEMS
(ENGINE-OUT, PAD-HOLD DOWN, VERIFIED STRUCTURAL MARGIN,)
- CREW SAFETY MAY IMPOSE
 - HIGHER MARGINS THAN NEEDED FOR AN OPTIMIZED COST EFFECTIVE UNMANNED SYSTEM
 - REDUNDANCY TO ENHANCE CREW ESCAPE POSSIBILITY (DETERMINED THROUGH ANALYSIS)
- ABORT SENSING AND IMPLEMENTATION SYSTEM IS NEEDED TO FILL THE GAP BETWEEN 100% RELIABILITY AND SYSTEM RELIABILITY
- GENERAL GUIDELINES AVAILABLE. PARTICULAR REQUIREMENTS ARE HIGHLY MISSION SENSITIVE

CONTINUING ACTIVITIES



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- COMPLETE ONGOING CONCEPT DEFINITION & EVALUATION
 - LRB FOR PLS
 - SHUTTLE-C PROPULSION APPLICATION
 - COST DATA FOR SELECTED CONCEPTS
- ET-CORE LAUNCHER SYSTEM
 - TWO LRB'S
 - LRB PROPULSION SECTION TECHNOLOGY FOR ET
 - VARIED PAYLOAD CAPABILITY
- ASSESSMENT OF LRB APPLICATION TO CURRENT PLANS FOR
FUTURE LAUNCHERS
- FINAL REPORT & DOCUMENTATION OF CONCEPTS